

TRANSIT BOOK

**Engineer's  
Field Transit  
Book**

MADE IN U. S. A.

Check Levels Mulberry Rd Bridge. Pg 1

Check levels Mulberry Rd Bridge

Aug 1967 Pg 4&5

July 1968 Pg 6&7

May 1970 Pg 8&9

Base Line W. abut 8

" " E. " 17

3-14-66  
 H. Patterson  
 R. Diedrich +

Check Levels  
 Mulberry Rd. Bridge  
 H.T. - Elev.

9/3/8 1

BM #	8.52	937.85		929.33
T.P.	0.17	925.99	12.03	925.82
			6.37	919.62
			9.10	16.89
			10.53	15.46
			11.79	19.20
T.P.	5.52	919.30	12.21	913.28
			8.76	10.54
			9.91	09.39
			10.20	09.16
			10.71	08.59
			9.37	09.93
			4.43	915.87
			5.60	10.70
			10.00	09.30
			10.90	08.40
			10.55	08.75
			10.24	09.06
			9.55	09.75

Hort. spk S. side CEI # 380303

12' E. OF SW. Wing wall

15' " " " " "

18' " " " " "

25' " " " " "

37' " " " " " & creek

50' " " " " "

56' " " " " "

60' " " " " "

67' " " " " " at base of footer

67' " " " " " on footer

18' W. of NE. Wing wall

35' " " " " " & creek

39' " " " " "

42' " " " " "

48' " " " " "

50' " " " " "

919.30

TP 12.78 929.01 3.87 916.23

T.P. 9.63 937.85 0.79 928.22

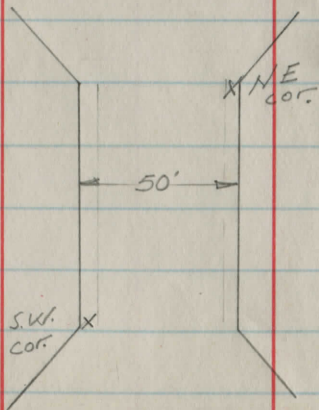
BM #2 8.53 929.32



Check Elev. Mulberry Rd  
 Bridge

1967

	+	HI	-	clev
BM	0.51	929.84		929.33
T.P.	0.51	918. <sup>9</sup> 88	10.47	918. <sup>9</sup> .37
			4.60	
			8.70	
			9.93	
			10.31	
			10.60	
			9.40	
			8.96	
			7.70	
			4.37	



Bob Kasie  
 Don Kasie  
 Paul Ranney

4

Spk S. side CEI # 380303

Top footer N.E. Cor

Bottom " " " " base

18' W of N.E. cor (face of wall)

21' " " " " " " " edge creek

35' " " " " " " " " "

39' " " " " " " " "

42' " " " " " " " " edge creek

46' " " NW cor Bott. footer base

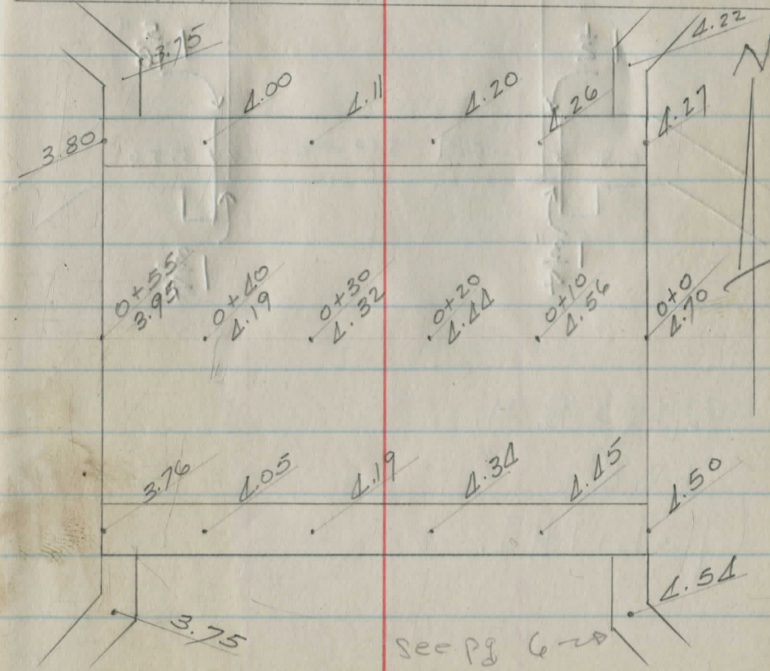
50' Top footer NW cor

See following page for S. end

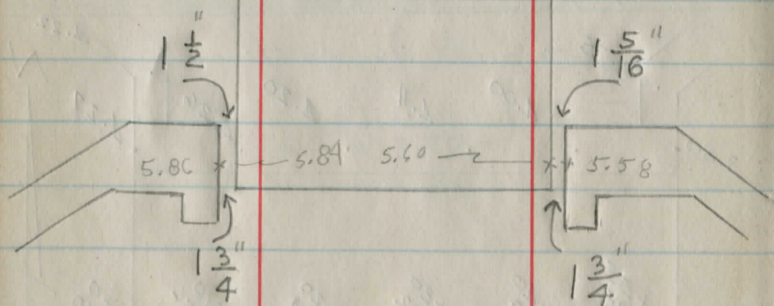
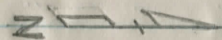
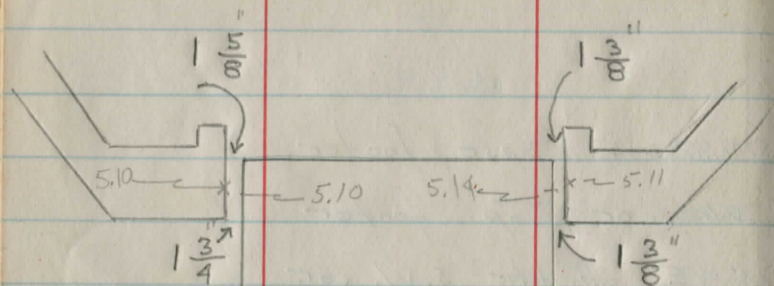
+	HI	-	c/cy.
	912.88		
	5.11	914.77	S.W. cor base footer
	4.10	915.78	S.W. cor Top footer
	6.72	913.16	12' E of the S.W. cor
	10.20	909.68	24' E. " " " "
	10.25	909.63	28' " " " " " edge creek
	10.80	909.08	35' " " " " " " "
	11.25	908.63	46' S.E. cor Footer base & edge creek
	4.60	915.28	50' Top footer S.E. cor

Top of Bridge

HI = 937.77



Sec Pg 6-20



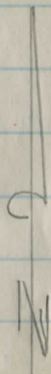
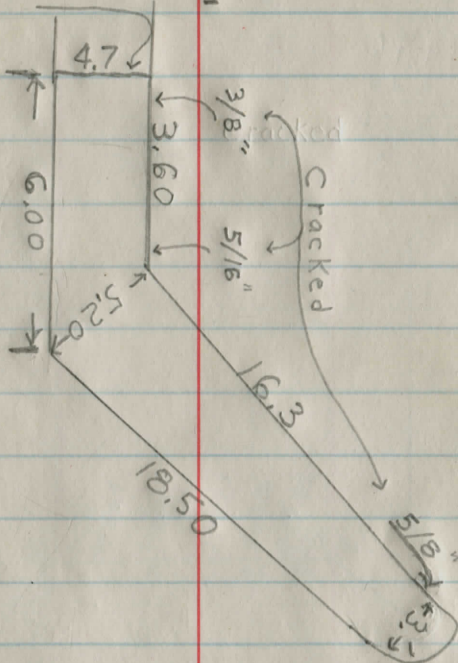
929.33 B. M.

+ 9.78

939.11 H.I.

S.E. Cor. Bridge

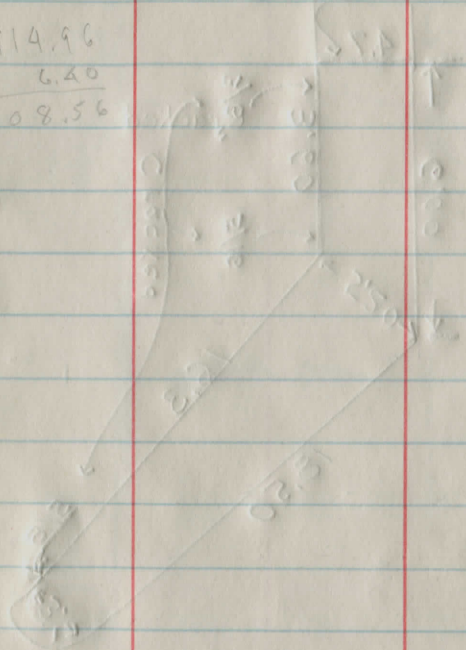
Cracked 1" +



©

Bob Kosie  
Don Kosie  
Bob Dedrich  
7/11/68

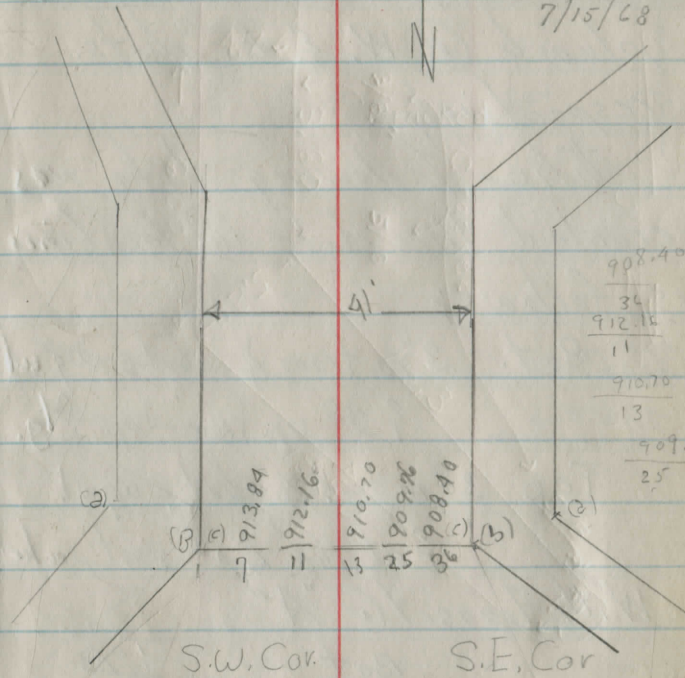
914.96  
 6.40  
 908.56



B.M. S. side C.E.I.

# 380303

Bob Kossie  
 Don Kossie  
 Bob Dedrich  
 7/15/68



(a) 913.84  
 7 11 912.16  
 13 25 910.70  
 32 909.26  
 36 908.40

908.40  
 34  
 912.16  
 11  
 910.70  
 13  
 909.26  
 25

(a) Top Footer + Face wall 915.87 (a) Top Footer + Face wall 915.37  
 (b) Top Footer East 915.60 (b) Top Footer West 914.96  
 (c) Base Footer + Edge curb bel 914.68 (c) Base Footer + Edge curb 908.56

#39 Bridge

@ Chagrin River

Pts "A" & "C" used to ck  
plumb @ W. & E. abuts.  
respectively.

The following data was  
recorded this date @ locations  
as follows:

Bot. 3" in from  $\Delta$  abut & wgw  
& 2" up from top ftg.

Top 3" in from  $\Delta$  abut & wgw  
& at the  $\Delta$  of seat pocket.

With transit @ "A"

	Bot	Top
S.W.	0.215	0.195
N.W.	0.200	0.140

With  $\pi$  @ "C"

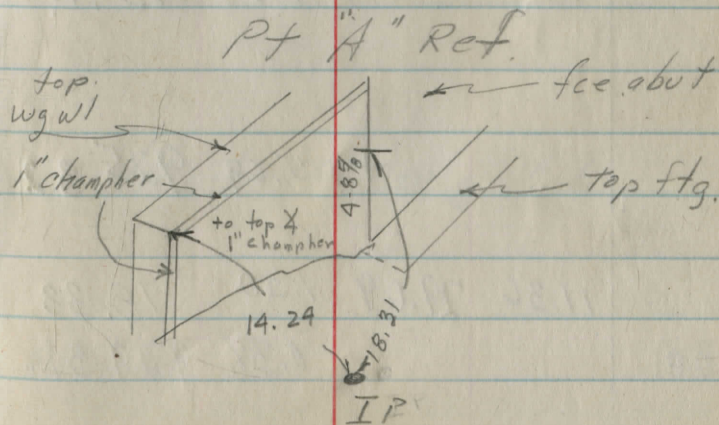
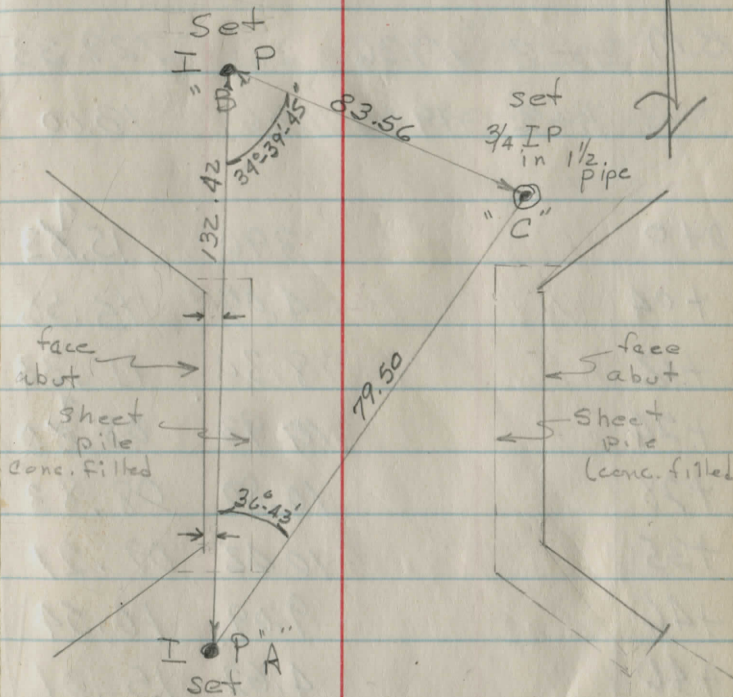
SE.	0.125	0.200
N.E.	0.400	0.495

Design-fee to fee abut - 50.75'

R.A. Davidson  
S.A. Merri H

Sunny-warm  
85° 8

May 14, 1970



#39 @ Chagrin River

X Sect. Stream @ S.

B.M. 0.03 929.36 929.33

1.63 19.63 11.36 18.00

0+0 3.90 15.83

+04 4.07 15.56

+12 8.30 11.33

+24 10.93 08.80

+28 10.80 08.83

+35 10.42 09.21

+46 9.09 10.54

+40 4.62 15.01

+50 4.52 15.11

+ 5.69 925.32

11.36 29.69 11.30 18.33

B.M. 0.38 929.31

R.A. Davidson  
S.A. Merritt

ptly. cldy - warm  
75° 9

edge deck (= drip line) 5/15/70

Hd. gpk. S. side C.E.I. # 380303

0+0 = fce W. abut  
top ftg.

dn

up

Top stt pile ret well @ S.E. X.

ck 0.02

#39 @ Chagin River

Ref pts. as pg 8  
dated 5/14/70

With  $\pi$  @ "C"

NE	Bot	Top
N.E.	0.400	0.495
S.E.	0.171	0.200

With  $\pi$  @ "A"

N.W.	0.200	0.140
S.W.	0.215	0.191

Davidson  
Merritt

8/26/70

Sunny warm. 10  
75<sup>10</sup>

@ S.W.  $\pi$  seat  
6" below bot deck  
spill 0.17 open  
from bkwl.

no change since 5/14/70

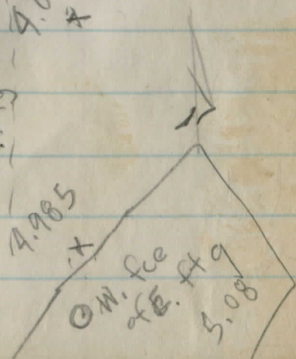
no change since 5/14/70

top flg  
@ abut \*4.578  
10' abt  
below dip line  
\*9.26 W. flg

E. flg - 9.863  
\*

4.985  
\*

@ W. flc  
\*E. flg  
5.08



#39-4.35-4

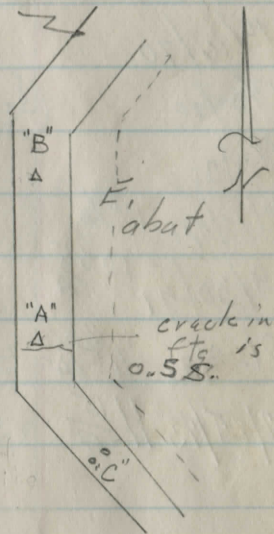
Fce to Fce obs. dim.

Date	Temp	N <sub>i</sub>	Corr S.	Corr
8/31/70	69°	50.53	—	50.35
10/14/70	48° <sup>25% A</sup>	50.54	50.53	50.35 50.34
12/30/70	130° = 25°	No meas. this date. no viz change evident		
4/5/71	35° 1/P	no fce to fce meas taken		
4/13/71	12 50/P 55°	50.53	-0.002 50.526	-0.004 50.35 50.346

(11)

@ X wgw to about-top of exst'g ftg.

Date	Dist. Ref "A"	E. ftg
8/31/70	Pt. to Fce shrt. 1.495	Loc. PK nail 4' N. of 5EA
10/6/70	1.500	
12/30/70	(see opp. pg.)	
4/7/71	1.530	(135°) 1/P
4/11/71	1.530	1120° A
9/30/71	1.530	1055° A
2/29/72	1.535	1120° A ±40°
4/25/73	7.565 1.55	1115° A 75°



(1/a)

39-4.35-4

Obs. Dim @ E. about See pg 11

Date	Dist. Ref. PT "B" to fce sht	Loc.
8/31/70	1.510	PK nail 7.18'S. of NEX
10/16/70	1.505	
12/30/70	(see pg 11)	
4/7/71	1.535	
6/11/71 11 <sup>20</sup> / <sub>A</sub>	1.540	
9/30/71 10 <sup>55</sup> / <sub>A</sub>	1.535	
2/29/72 11 <sup>20</sup> / <sub>A</sub>	1.61	±40°
7/25/73 11 <sup>15</sup> / <sub>A</sub>	1.55 1.545	75°

39-4.35-4

(1/b)

Obs. Dim @ E. about See pg 11

Date	Dist. Ref. PT "C" to fce sht	Loc.
8/31/70	3.855	From fce. about. w.g. to fce. sht. pile 6.14'S. E. of S. E. X.
10/16/70	3.910	
12/30/70	(see pg 11)	
4/7/71	3.900	
4/11/71 11 <sup>20</sup> / <sub>A</sub>	3.910	
6/11/71 11 <sup>00</sup> / <sub>A</sub>	3.905	
2/29/72 11 <sup>20</sup> / <sub>A</sub>	3.95	±40°
7/25/73 11 <sup>15</sup> / <sub>A</sub>	3.95	75°

#39 @ Chagrin River

X sec stream @ S.

B.M. 8.87 938.70 929.33

0.46 27.85 10.81 927.39

2.72 19.06 11.51 16.34

0+0 3.33 15.73

+04 3.51 15.55

+04 4.60 14.46

+12 7.79 11.27

+24 10.09 08.97

+28 10.17 08.89

+35 9.83 09.23

+46 9.25 09.81

+46 4.06 15.00

+50 3.97 15.09

11.51 27.85 2.72 16.34

10.69 38.07 0.47 27.38

B.M. 8.74 929.33

R.A. Davidson Pkly. cloudy  
S.H. Merritt cool. 50°

edge deck (drip line)

splk. pole #380303

10/16/70 (12)

up

dn

dn

up

ck - 0.00

Note: gravel bar  
N. of struct.

remove to pt.  
± 150' N. of N side  
struct.

#39 @ Chagrin River

Ref pts. as pg 8 dated 5/14/70

With T @ "C"

	<u>Bot.</u>	<u>Top</u>
NE.	0.400	0.495
SE.	0.721	0.190

With T @ "A"

	<u>Bot</u>	<u>Top</u>
N.W.	0.200	0.130
S.W.	0.215	0.189

Dist. from Base Line A-B

N.W.	2.012	1.930
S.W.	1.178	1.165

Cldy-cool  
Davidson  
Merritt

50°  
10/16/70

(13)

Top. Htg @ abut - rod readings

0.815

x

x 1.100

//

x

0.600

x 1.215

#39 @ Chagrin River

Ref's pts as pg. 8

Dist from Baseline A-B

	<u>Top</u>	<u>Bot.</u>
N.W	1.930	2.015
S.W.	1.160	1.173

With  $\pi$  @ C

N.E	0.495	0.395
S.E	0.190	0.115

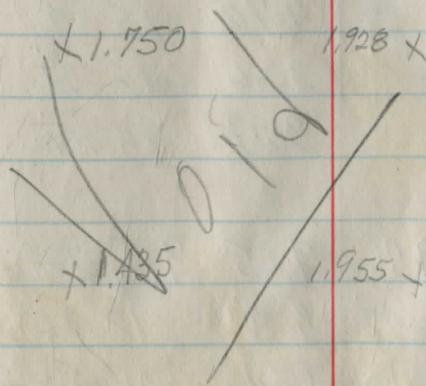
Ptly Clay - Worn 4/13/71  
Davidson  
Merritt

(14)

@ S.W. 6" seat  
below bot deck  
spill 0.19 open  
from bk wl. (see pg 10)

@ N.E & bkwl. broken  
From abut. in seat pocket  
& @ S.E & same

Top ftg @ abut - rod readings



# 39 @ Chagrin River

39-4.35-4

Davidson  
Merritt

Sunny-cool

9/19/71

(15)

X Sec Stream @ S. drip line

BM 7.65 936.98 929.33

0.47 26.18 11.27 25.71

3.32 18.77 10.73 15.45

040 3.06 15.71

+04 3.24 15.53

up

+04 4.34 14.43

dn

+12 7.14 11.13

+24 8.84 09.93

+28 9.48 09.29

+35 9.80 08.97

+46 9.39 09.38

dn

+46 3.77 15.00

up

+50 3.70 15.07

+50 3.56 15.21

N. drip line

040 3.27 15.50

" " "

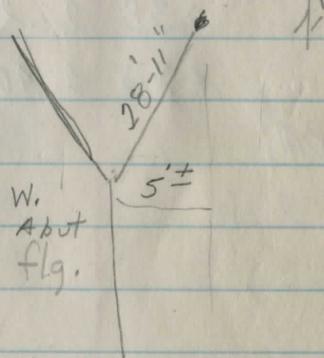
TBM#1 8.04 19.76 7.05 911.72

10.81 26.77 3.80 15.96

10.86 37.12 0.51 26.26

BM 7.76 929.36

SPK in Pole # 380303

TBM #1 Ref  
(Metallic Tape)  
(No plumb) I. PipeW.  
Abut  
flg.Top 3/4" pipe 4" above grd. Elev. 911.905  
see pg 16ck 0.03 N.G. USC X SEC.  
TBM Rerun see pg 16

Reron BM to

TBM #1 pg 15

BM.	1.200	30.530	929.330
	0.030	19.375	11.185
	3.540	14.675	8.240
TBM #		3.000	911.675
	8.830	18.915	4.590
	11.725	30.190	0.450
		1.025	29.165

ck N.G.

BM.	7.37	36.70	929.33
	0.38	26.23	10.85
	4.375	20.405	10.20
TBM #		8.70	911.705
		4.92	915.485
		5.19	915.215
		5.32	915.085
	8.49	20.195	8.70
	1.73	4	915.710
	10.21	24.675	1.73
	9.66	37.872	0.515
BM		8.50	29.165

described pg. 15

- NW. X
- N.E. X
- S.E. X
- S.W. X

ok 0.01 ok

#39-4.35-4  
 Mulberry @ Chagrin River  
 E. about Base

Observation of dist to  
 face about taken @  
 N.E.S. drip lines  
 (3' in from A about & up E 2' above top ftg.)

D - E

	Top	Bot
1 <sup>30</sup> / <sub>P</sub> N.E.	—	0.49 (-)
S.E.	—	0.575 (+)

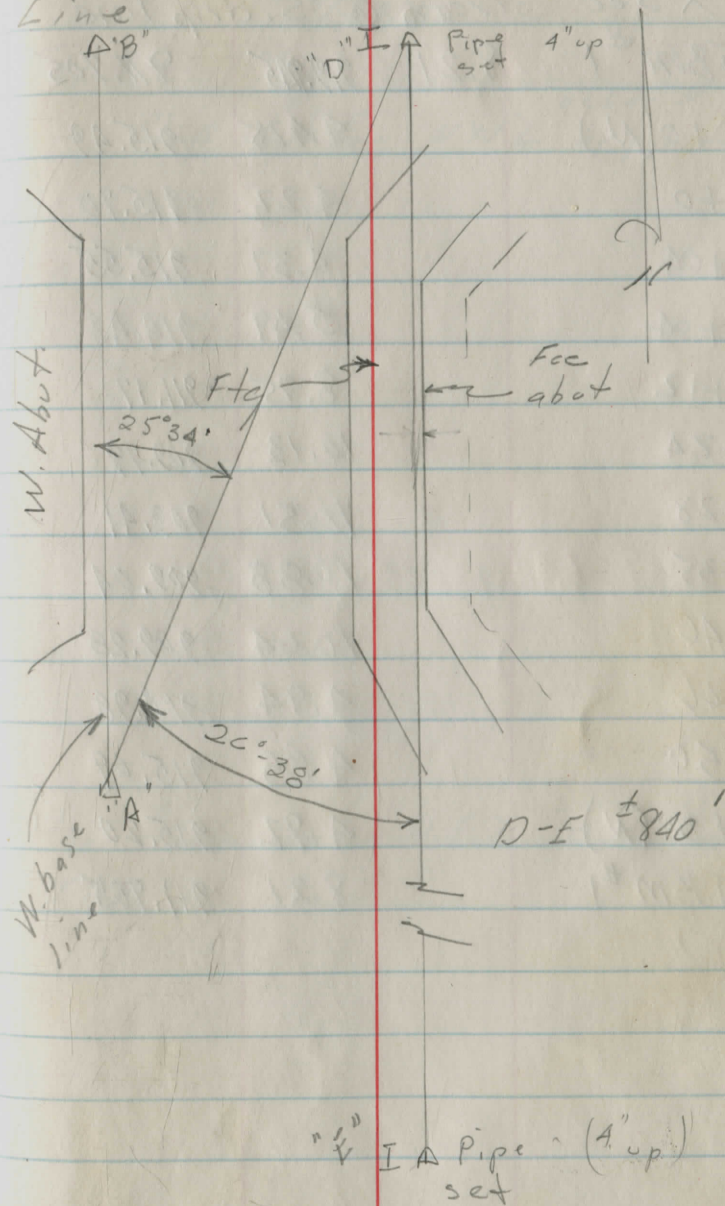
	Top	Bot
1 <sup>45</sup> / <sub>P</sub> A.B	—	2.015 (+)
N.W	—	1.175 (+)
S.W	—	

Darwin  
 Merritt

Sunny - warm 75°  
 6/11/71

17

Line  
 A'B"



"V" I A Pipe (A" up)  
 set

#39 @ Chagrin River

X Sec	Stream @ S. drip line		
TBM #1	8.21	919.915	911.705
0+0(N)		4.25	915.49
0+0		4.22	915.70
+04		4.37	915.55
+04		5.49	914.43
+12		8.75	911.17
+24		10.13	909.79
+28		10.51	909.41
+35		10.88	909.04
+46		10.64	909.28
+46		4.94	914.98
+50		4.85	915.09
+50(N)		4.72	915.20
TBM #1	8.21	911.705	

Davidson  
meritt #

cleav - top +  
± 80°  
9/30/71

18

Top 3/4" I Pipe

top ftg @ about face NW 4 drip line  
under N.

up

dn

dn

up

top ftg @ about face NE 4 drip line  
under N.

TBM #1

Chagrin River  
 @ #39 Profile Str. to S.

TBM #1	7.65	19.355	911.705		
		10.28	909.07	✓	
		4.37	914.98	✓	
0+0		9.65	909.70	✓	
		3.91	915.44	✓	
+50		9.45	909.90	✓	
1+0		9.19	910.16	✓	
2+0		8.66	910.69	✓	
2+50 = TP	6.48	18.365	7.47	911.885	✓
3+0		6.82	911.54	✓	
+50	?	7.95	910.41	✓	
4+0		6.93	911.43	✓	
+50		6.95	911.41	✓	
5+0		6.58	911.78	✓	
+50		6.33	912.03	✓	
6+0		6.98	911.38	✓	
+50		6.96	911.40	✓	
TP <sup>7+0</sup>	5.24	19.775	5.83	912.535	✓
		4.78	911.95		

Davidson  
 Merri H  
 Cldy - cool 2/29/72 19  
 ± 40°

see pg 15 for description  
 @ N. drip line ± of stream  
 E. Ftg. top @ fee under S. drip line  
 @ S. drip line ± of str.  
 W. Ftg. top @ fee under S. drip line  
 & River 0.40' = S. drip line  
 " 2 ft. paced dist. to S.  
 "  
 "  
 "  
 "  
 "  
 "  
 "  
 "  
 " ± Peterson S. P. on W. side  
 ± 6' E of River @ str. from W.

Profile to S.

17.775

7+50		6.10	911.67	✓	
8+0		5.16	912.61	✓	
+50		5.02	912.75	✓	
9+0		5.00	912.77	✓	
+50		5.00	912.77	✓	
10+00		4.95	912.82	✓	
TP <sub>3</sub>	5.55	20.155	3.17	914.603	✓
+50		7.16	912.99	✓	
11+0		6.95	913.20	✓	
+50		7.50	912.65	✓	
12+0		6.44	913.71	✓	
+50		5.70	914.45	✓	
13+0		6.03	914.12	✓	
TP <sub>4</sub>	2.96	17.42	5.69	914.46	✓
TP <sub>5</sub>	3.25	16.43	4.24	913.18	✓
TBM #1		4.78	911.65	✓	

4/29/72

20

£ River

"

"

"

"

"

"

"

"

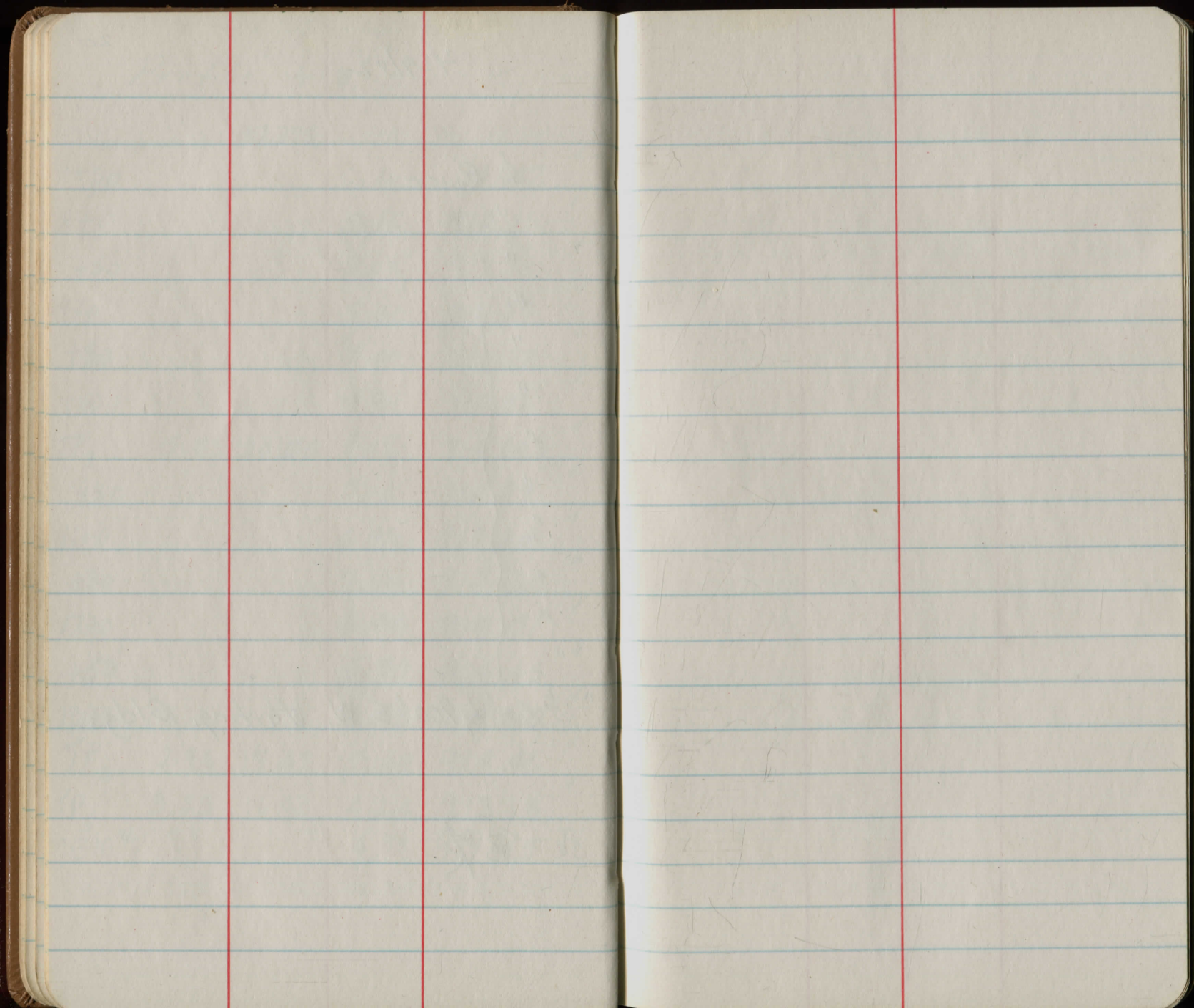
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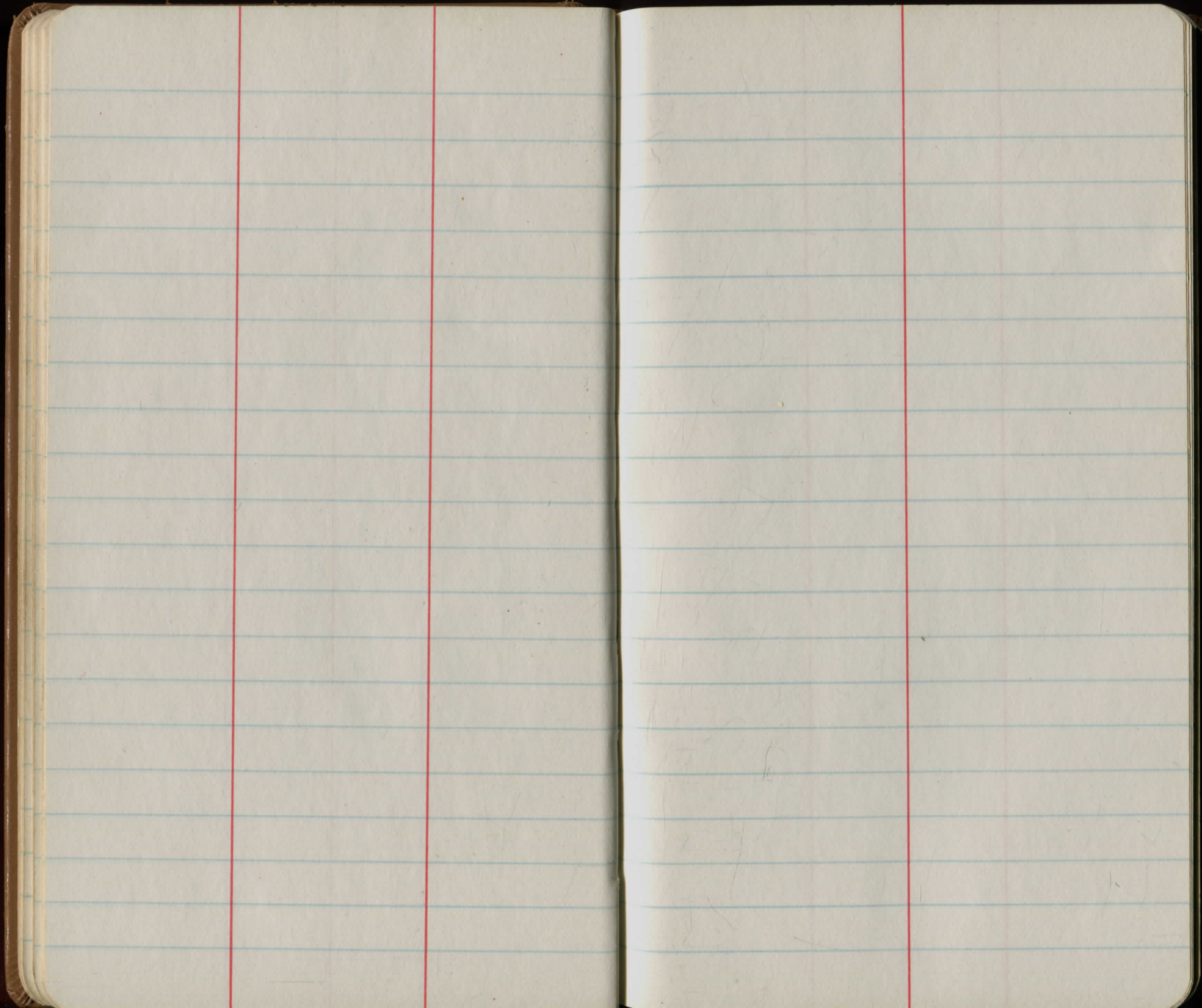
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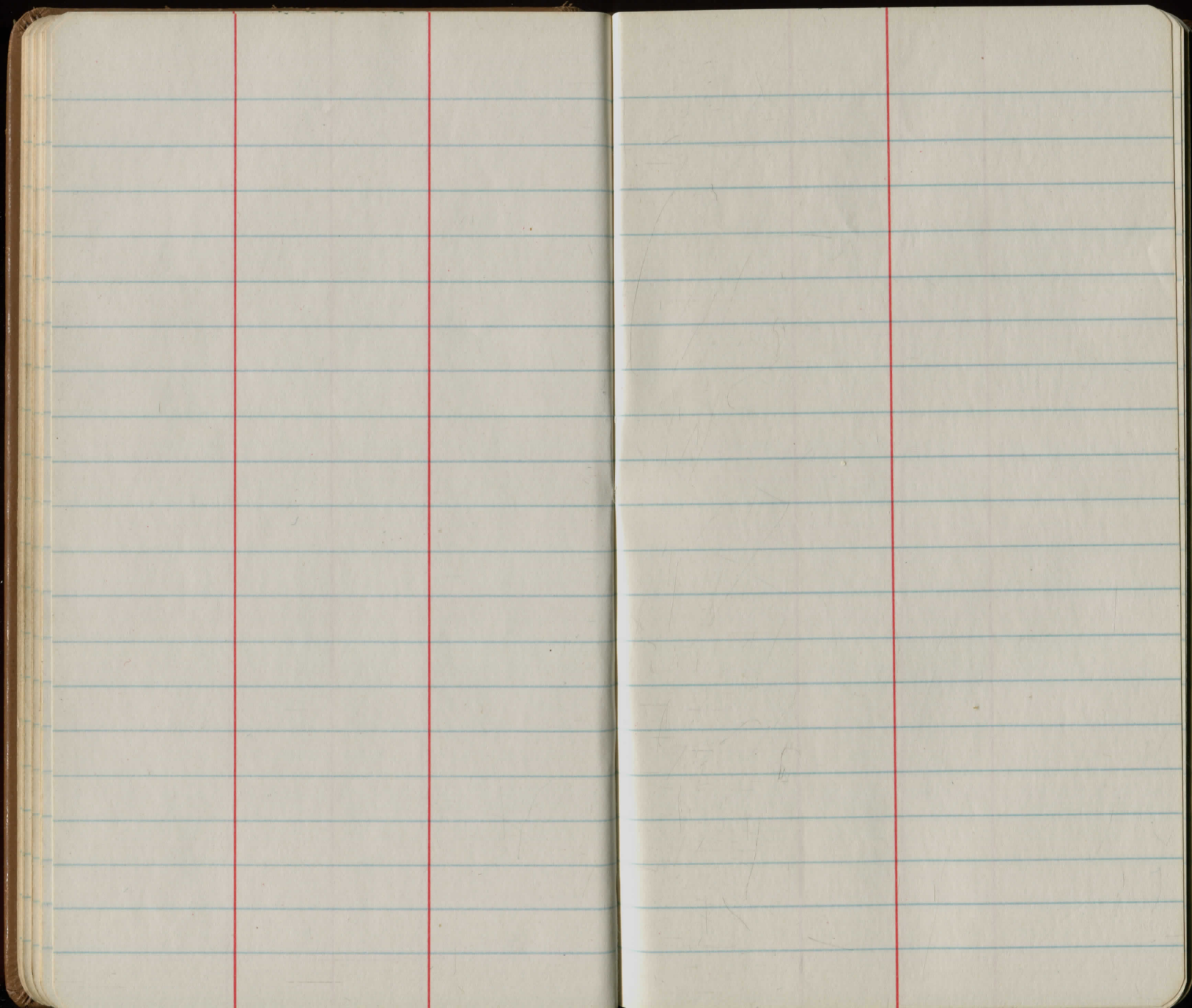
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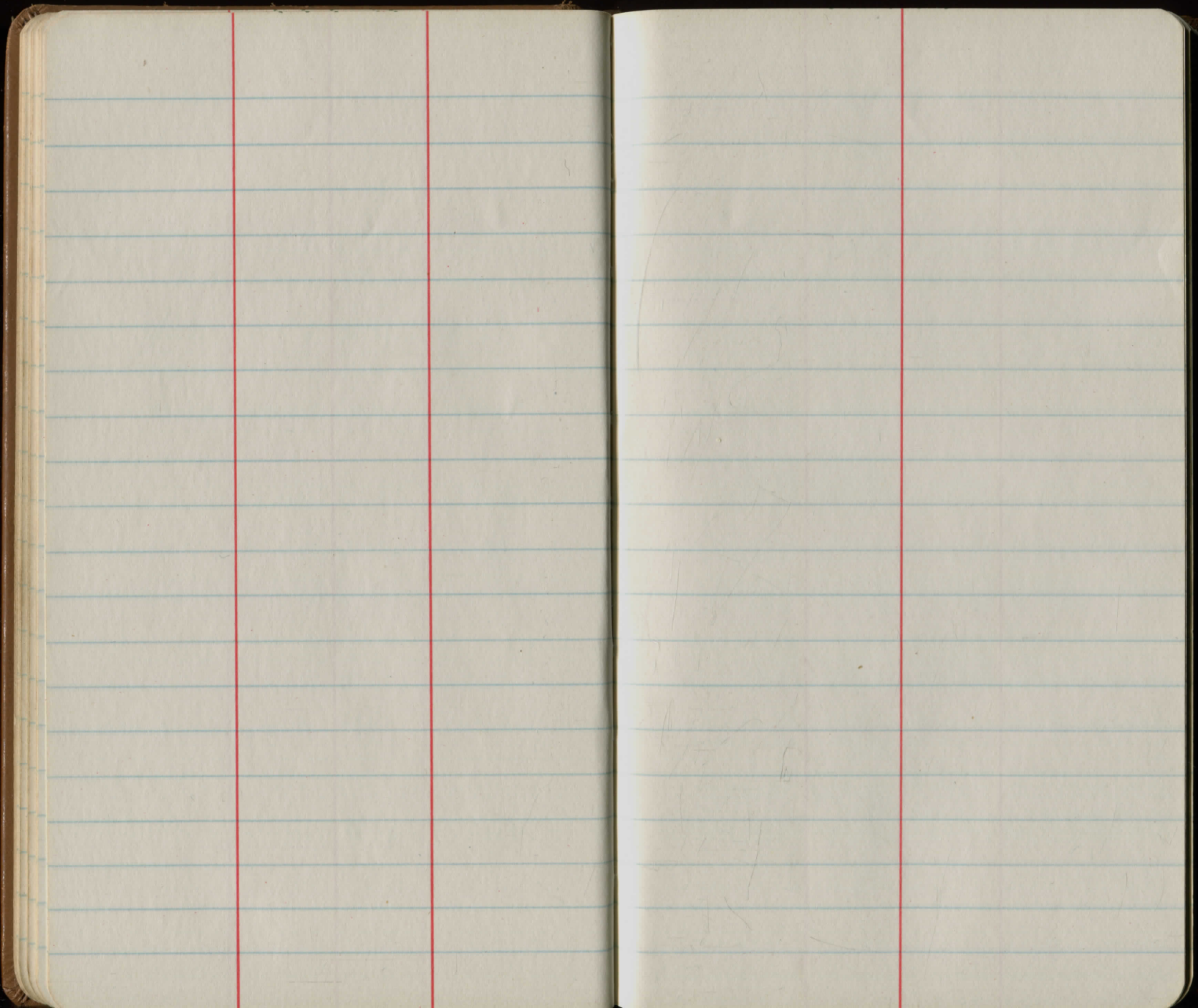
" ± 600' to 700' S.W. Whiting's Bldgs.

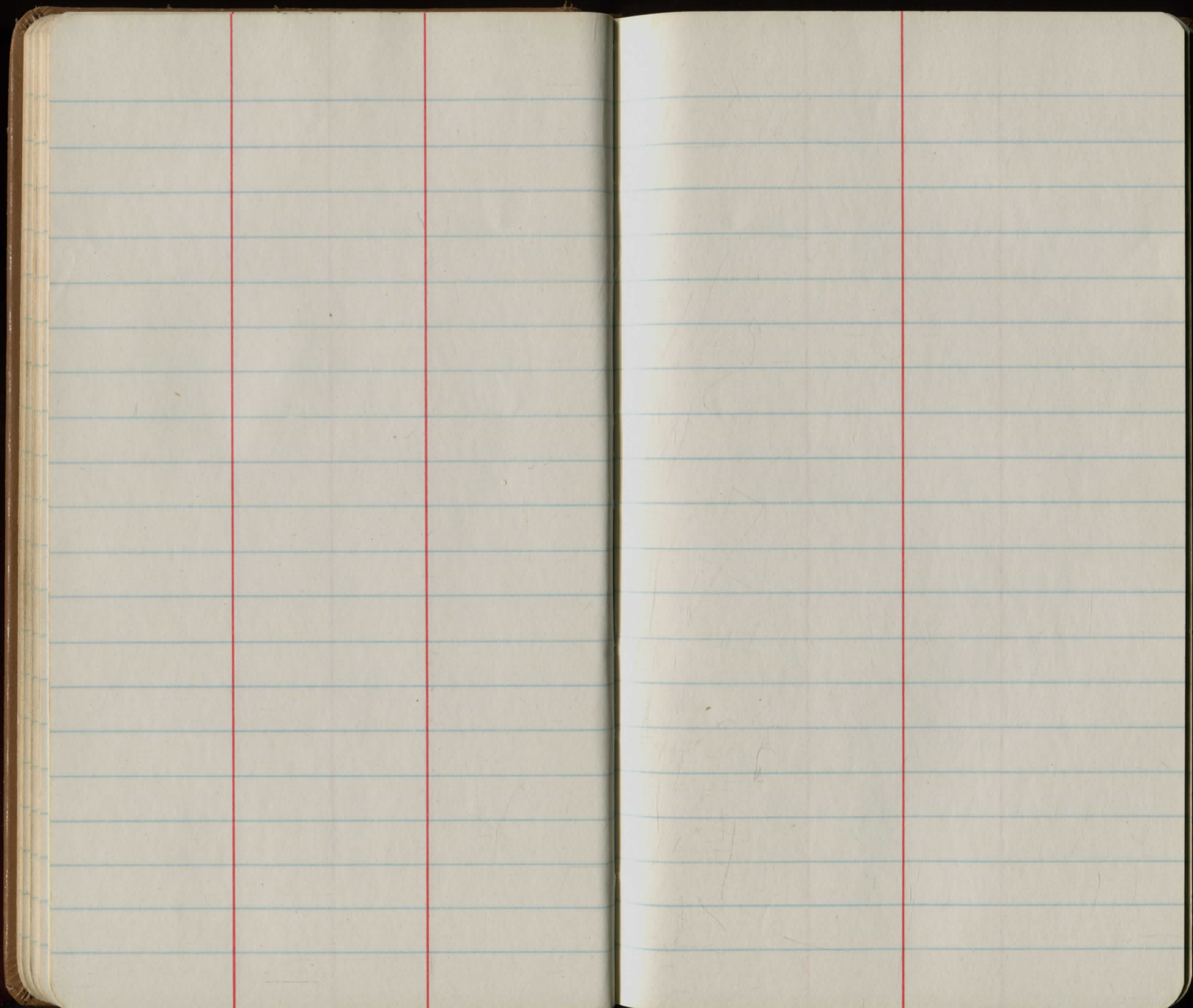
ck 0.05 %

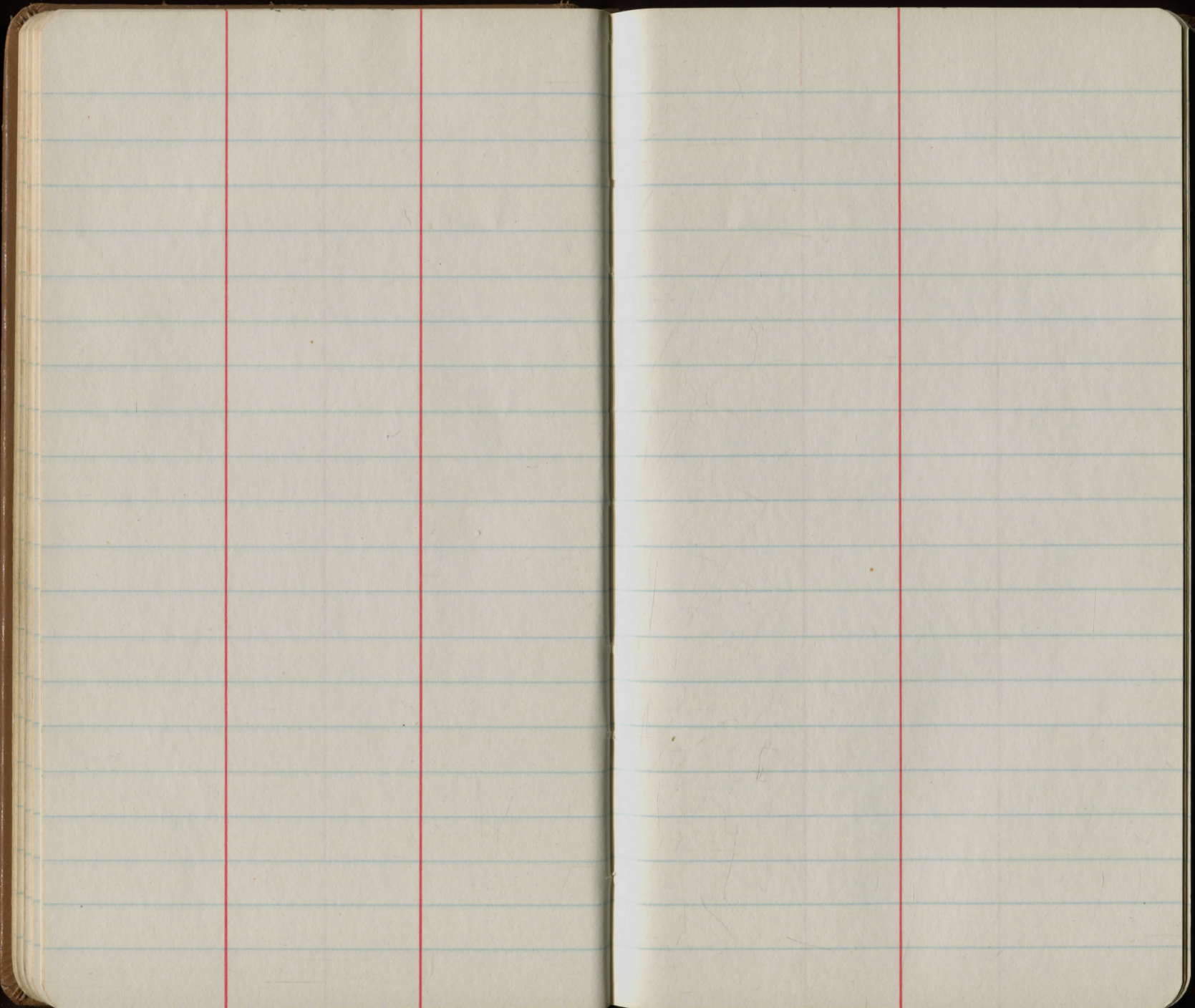


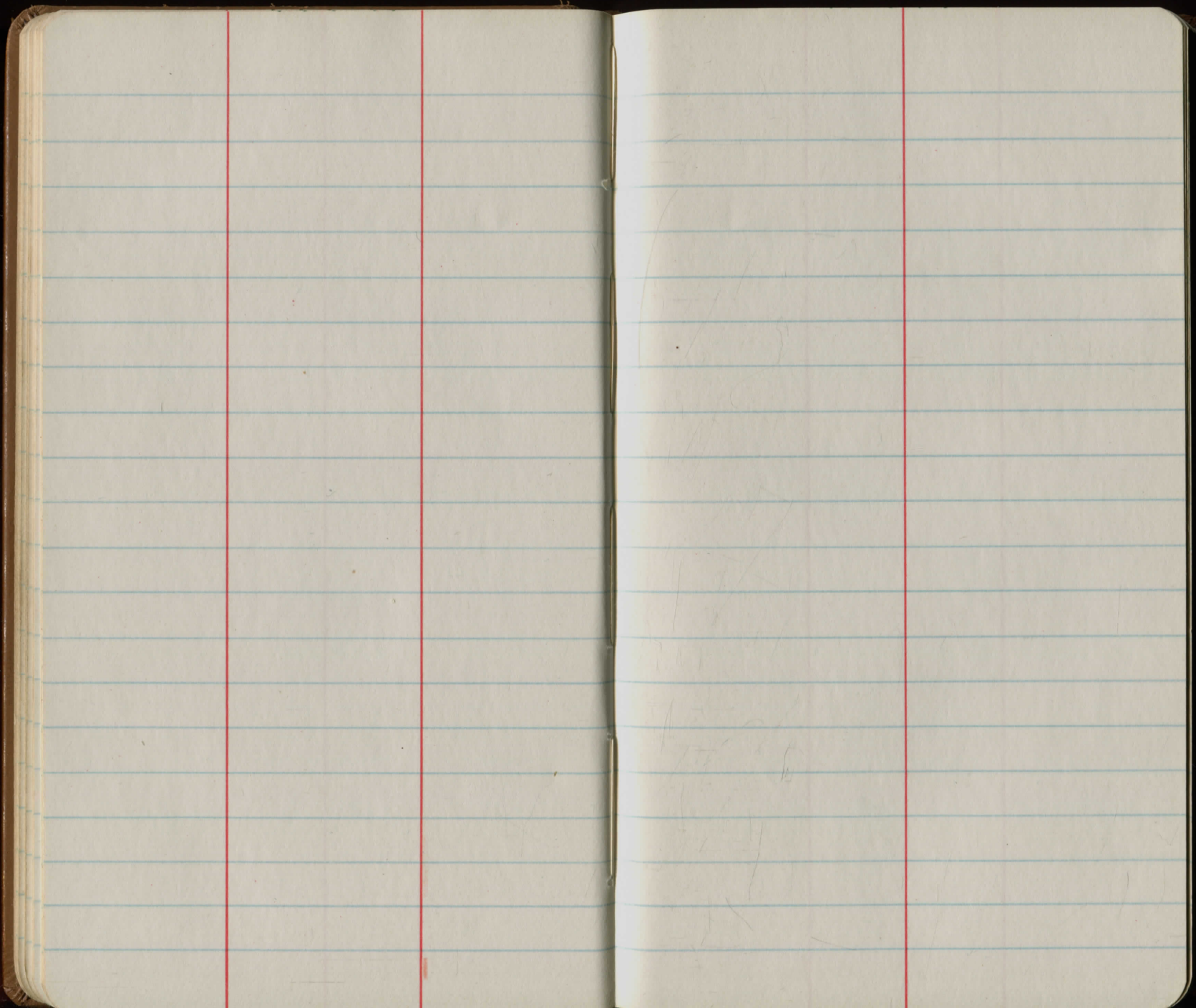


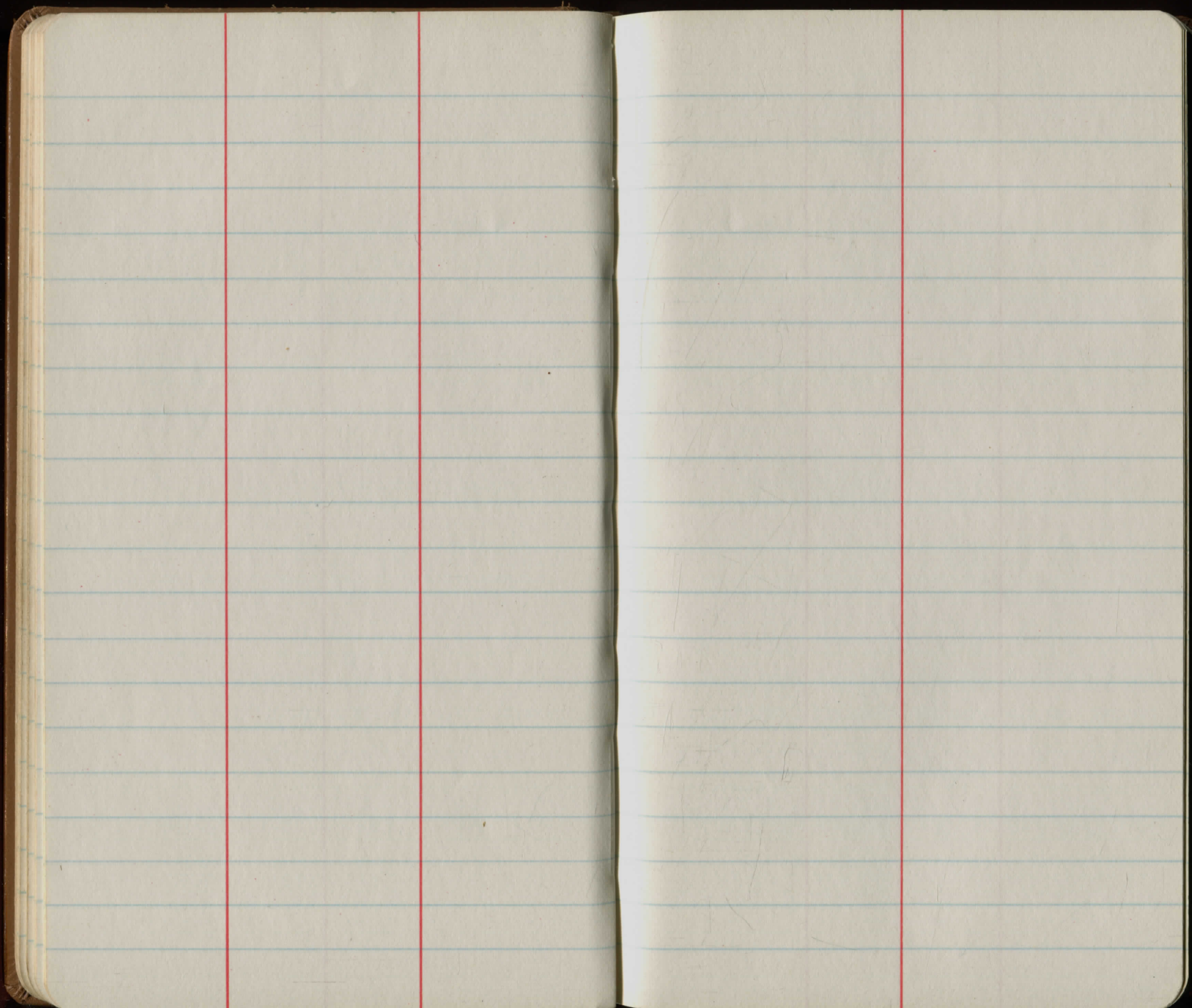


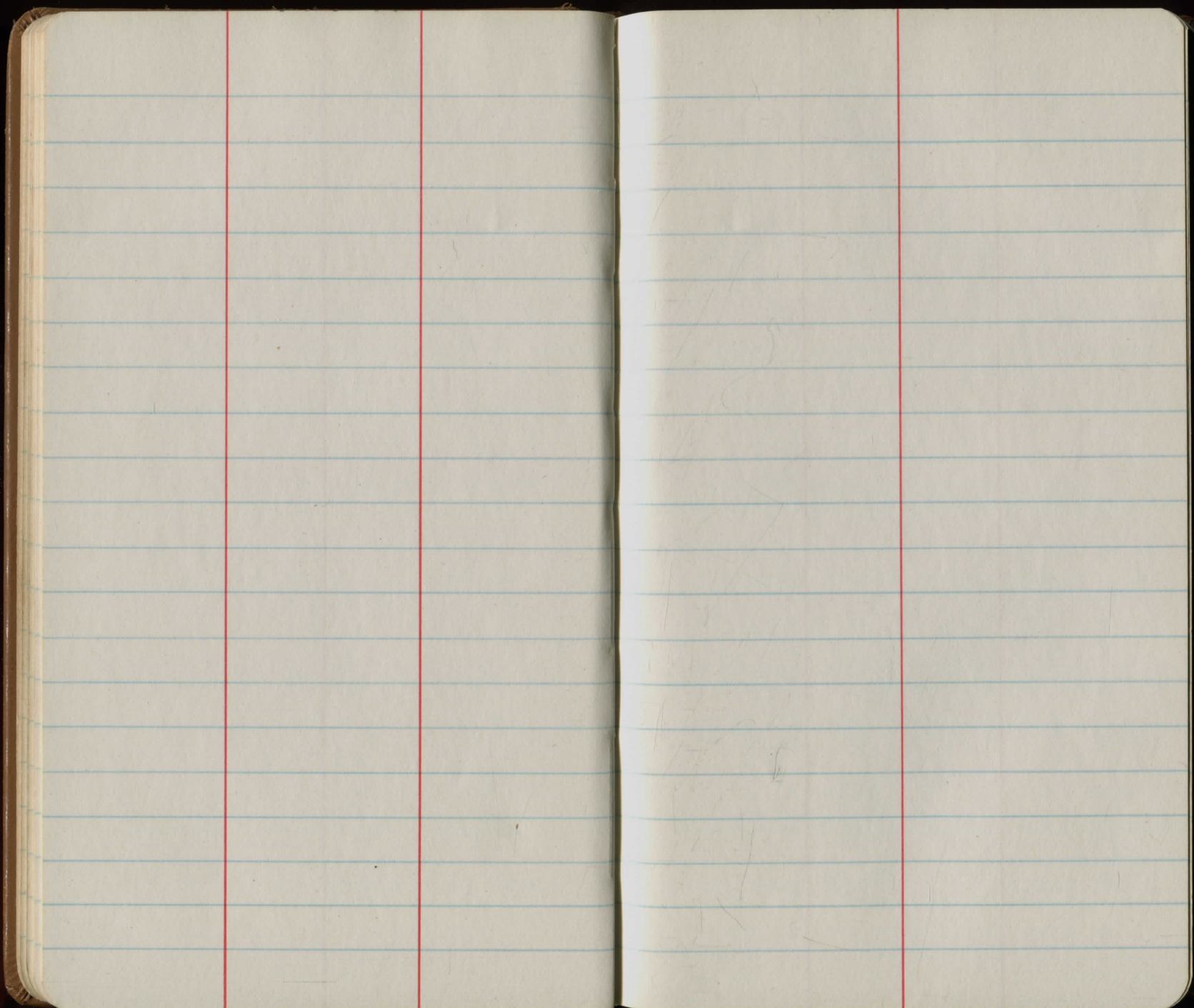


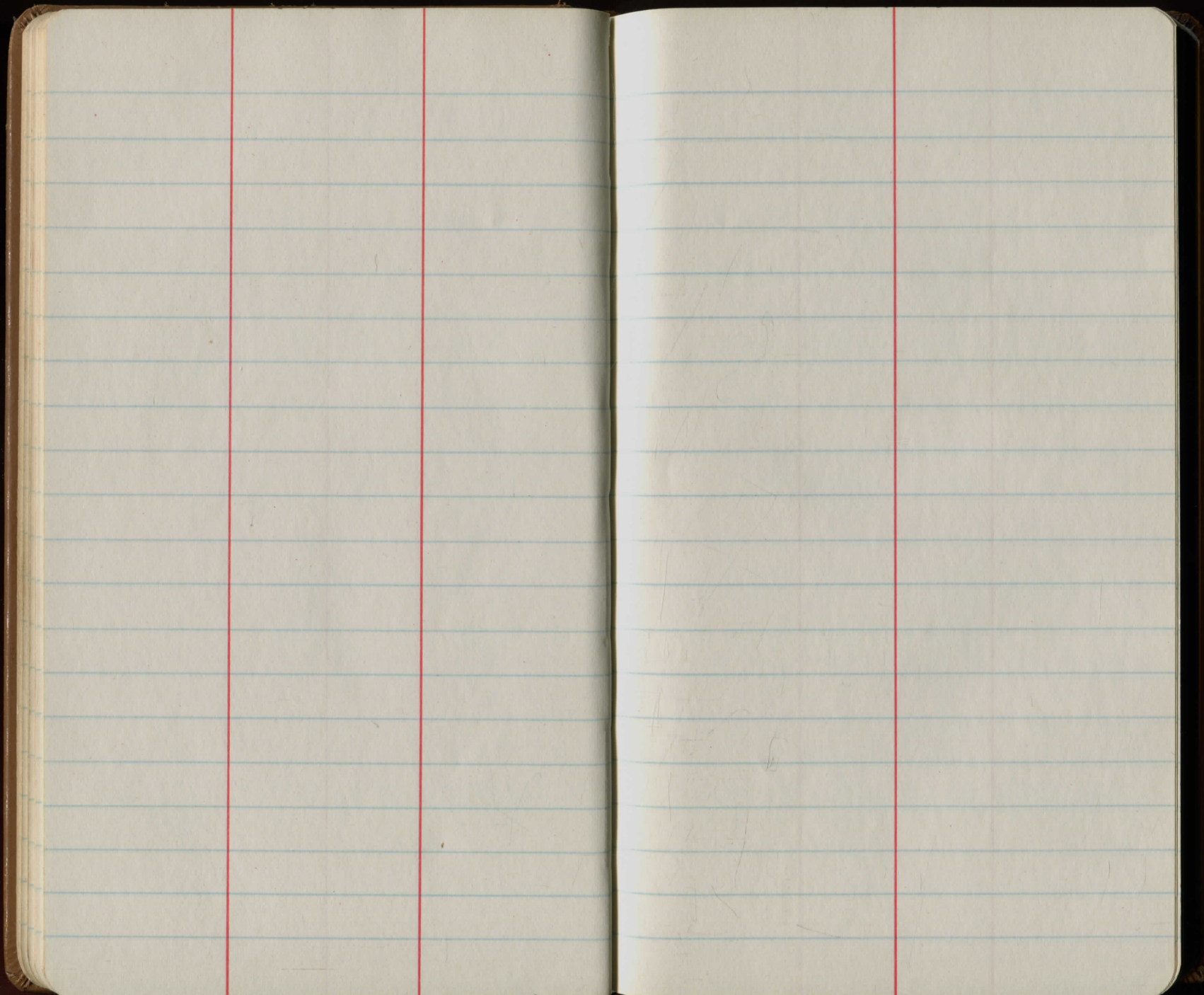


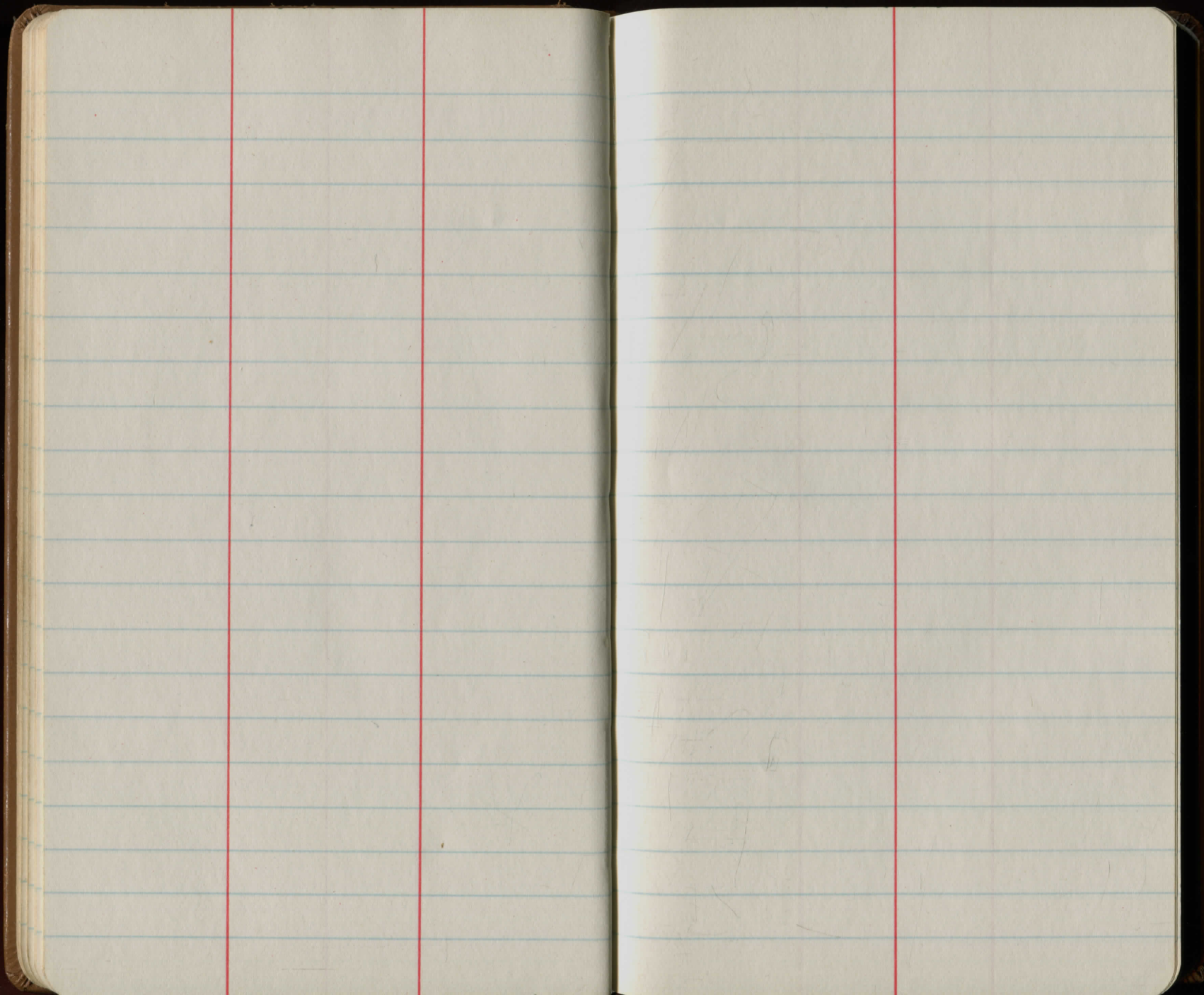


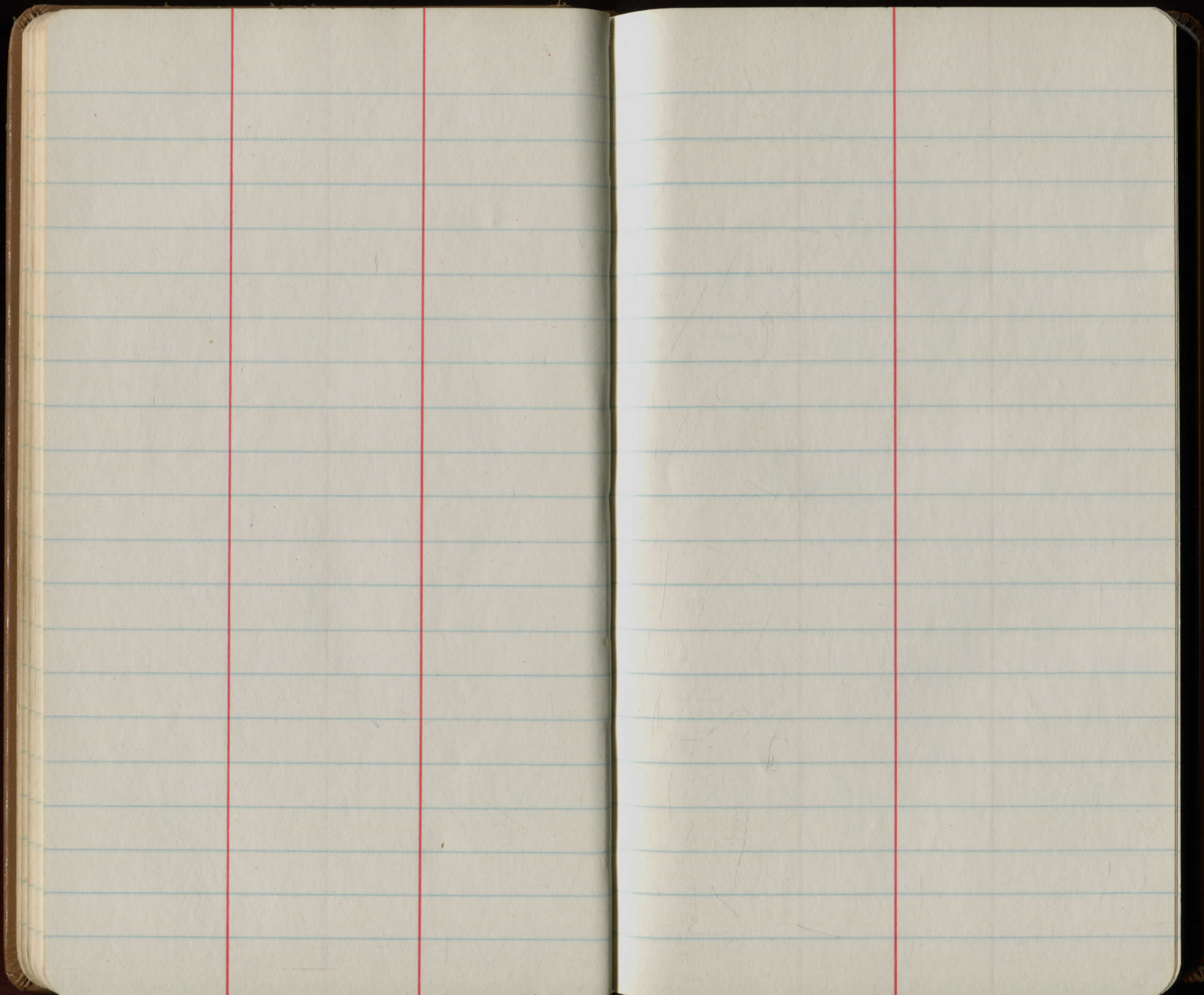


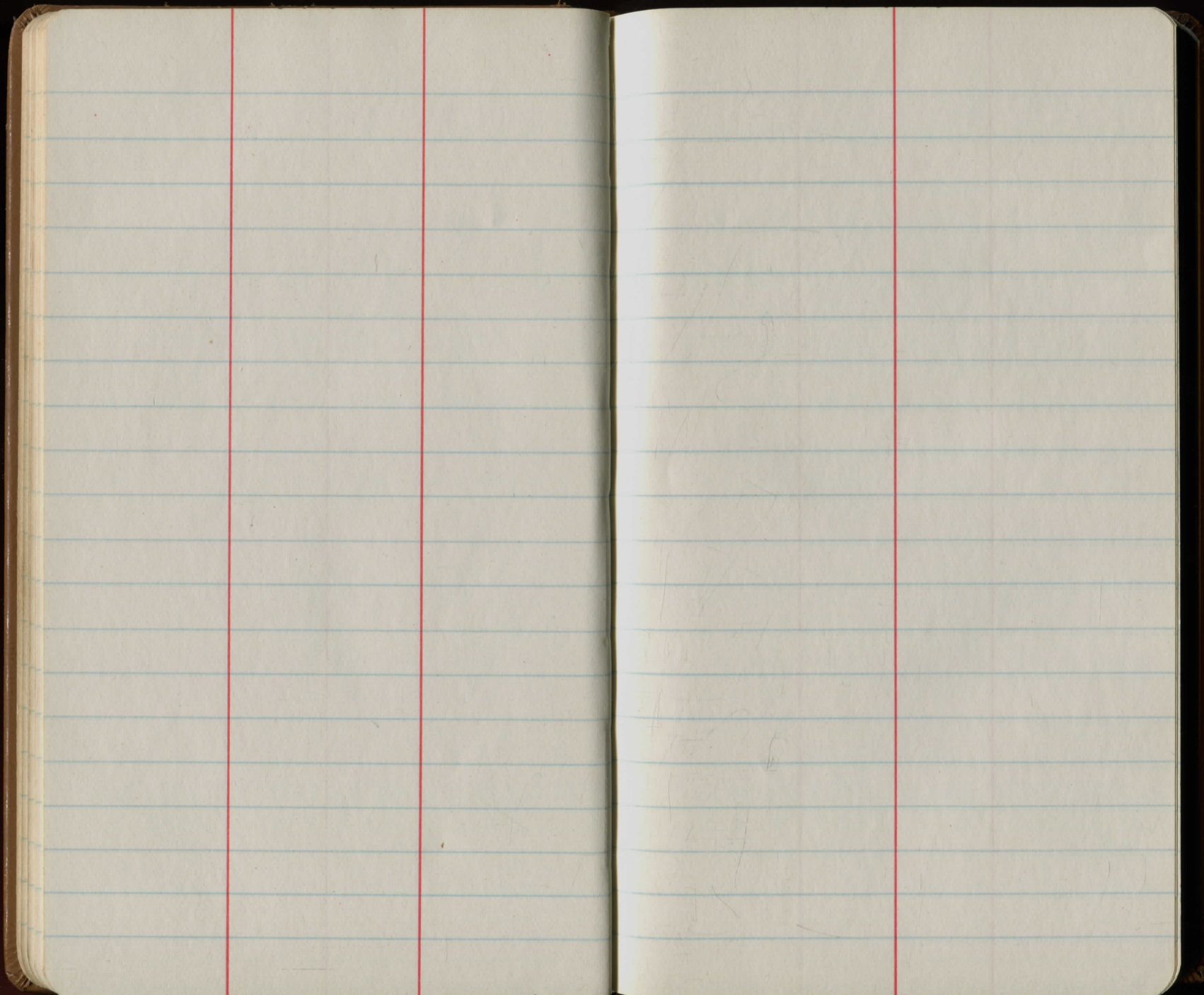


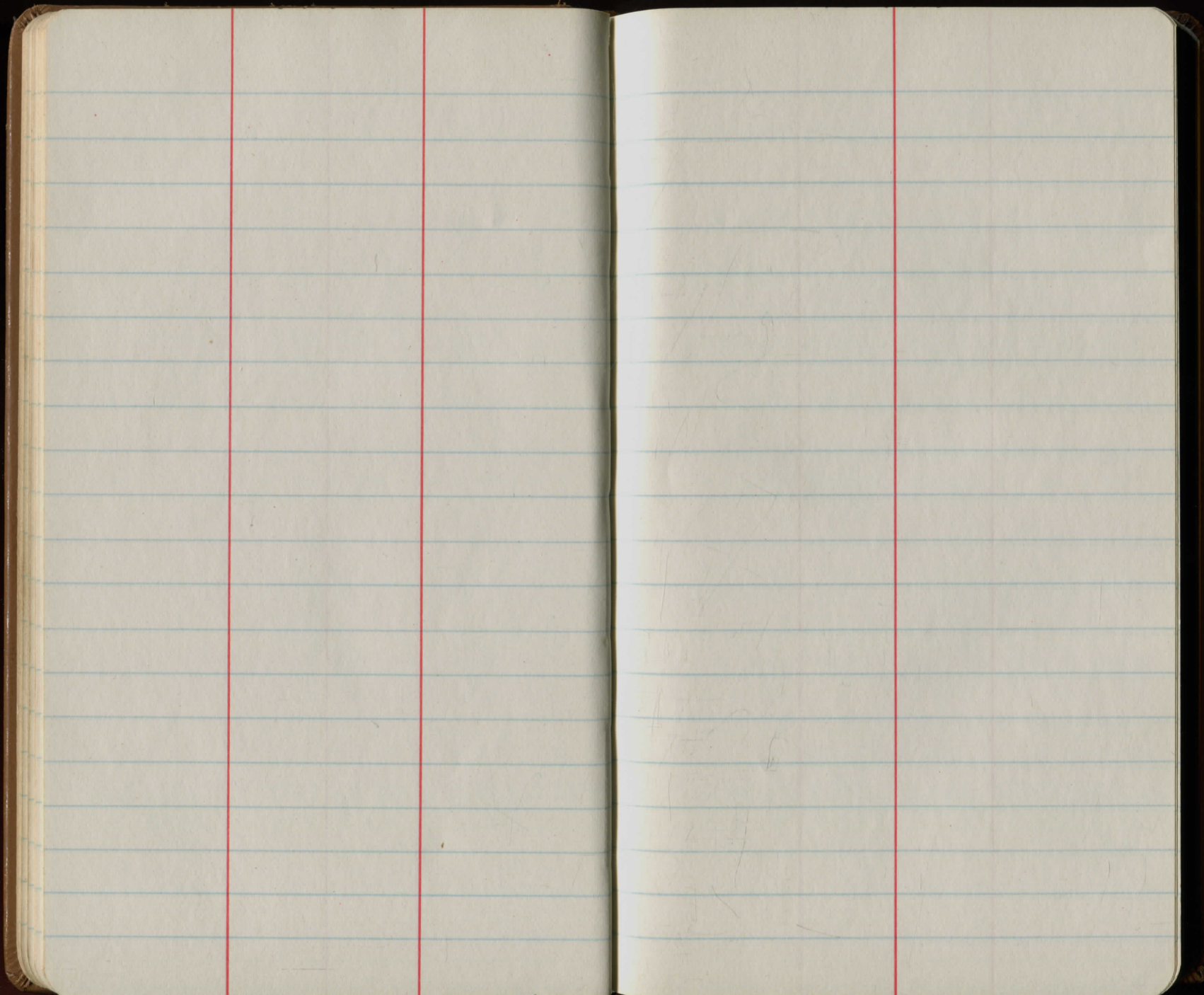


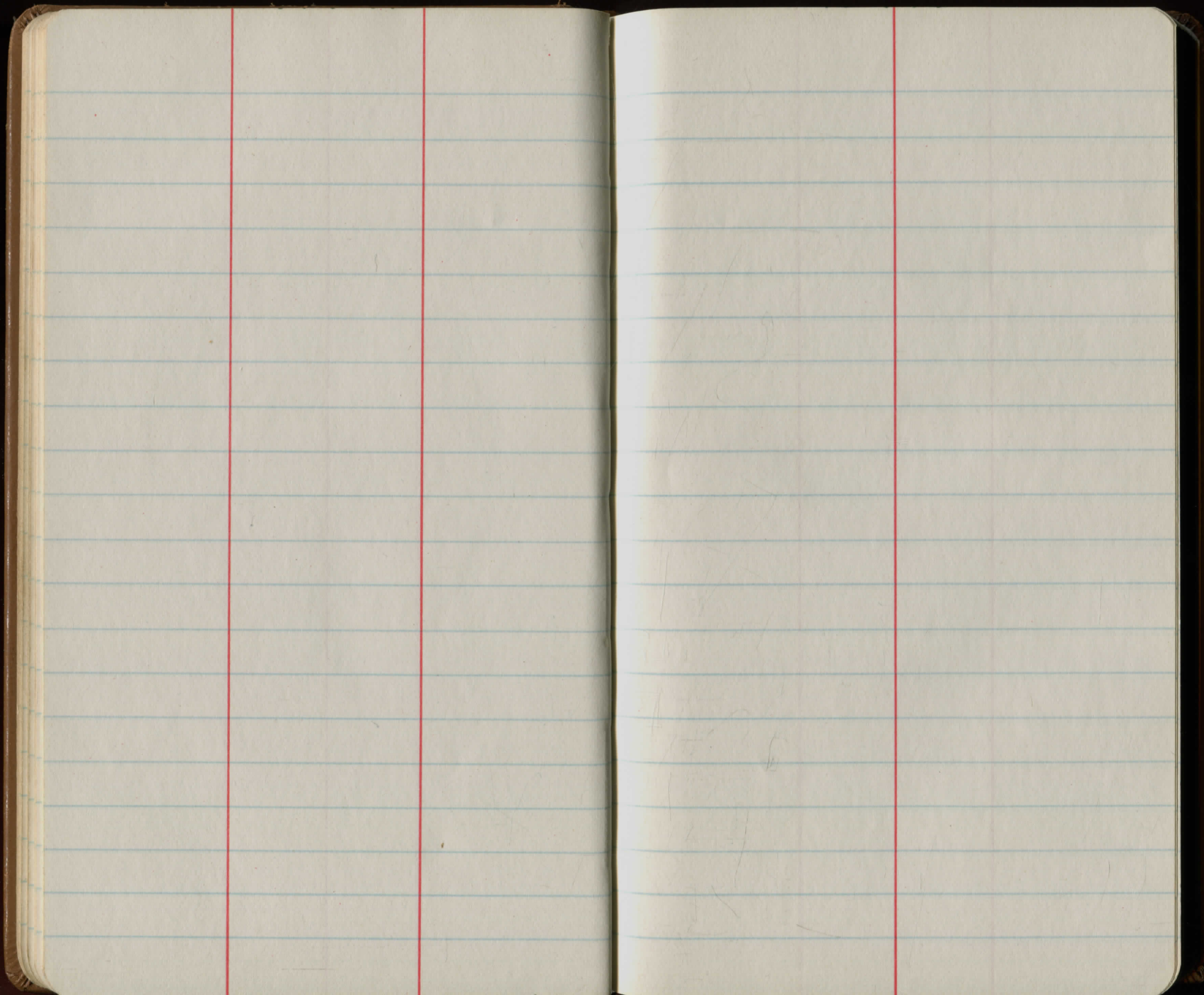


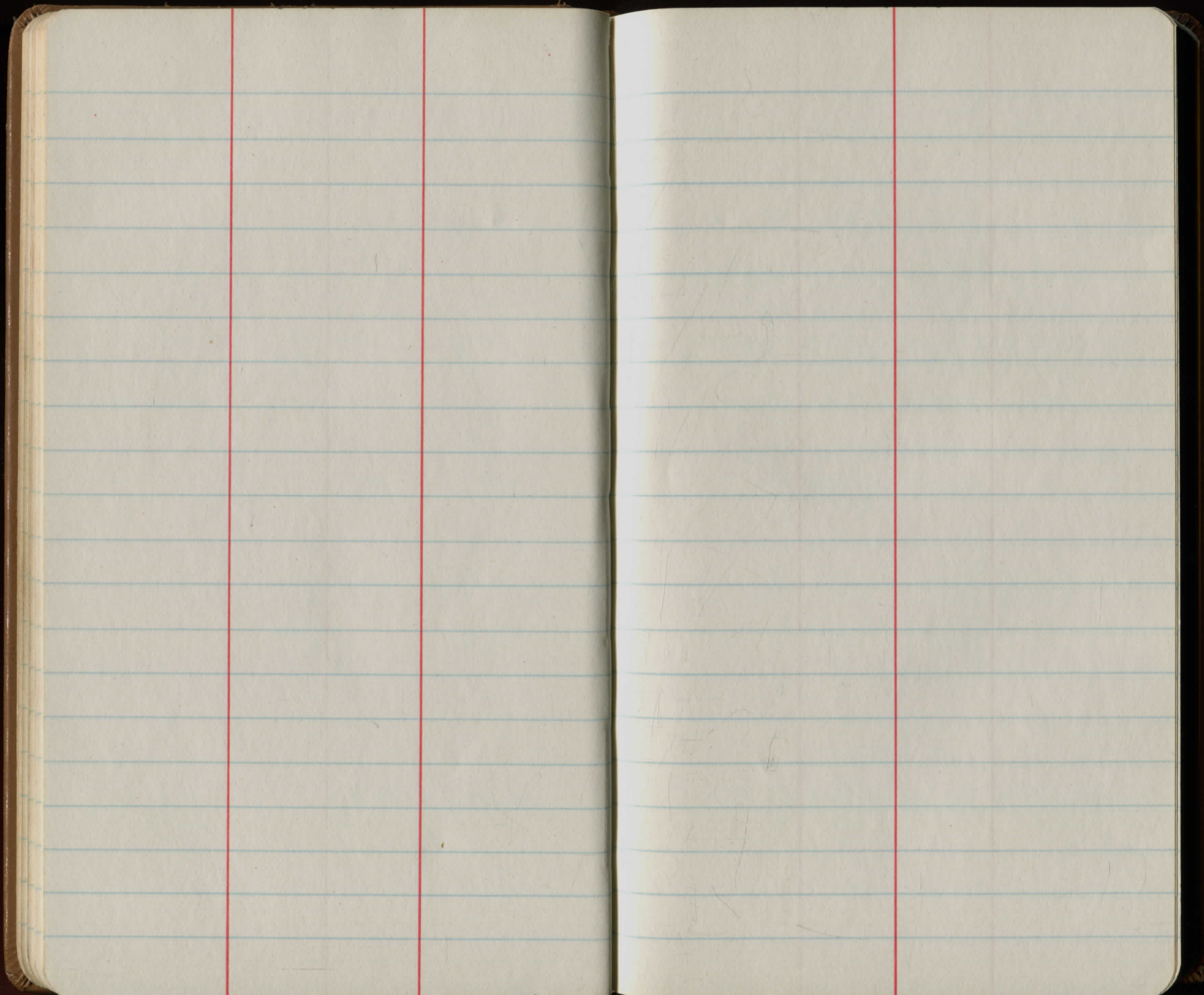


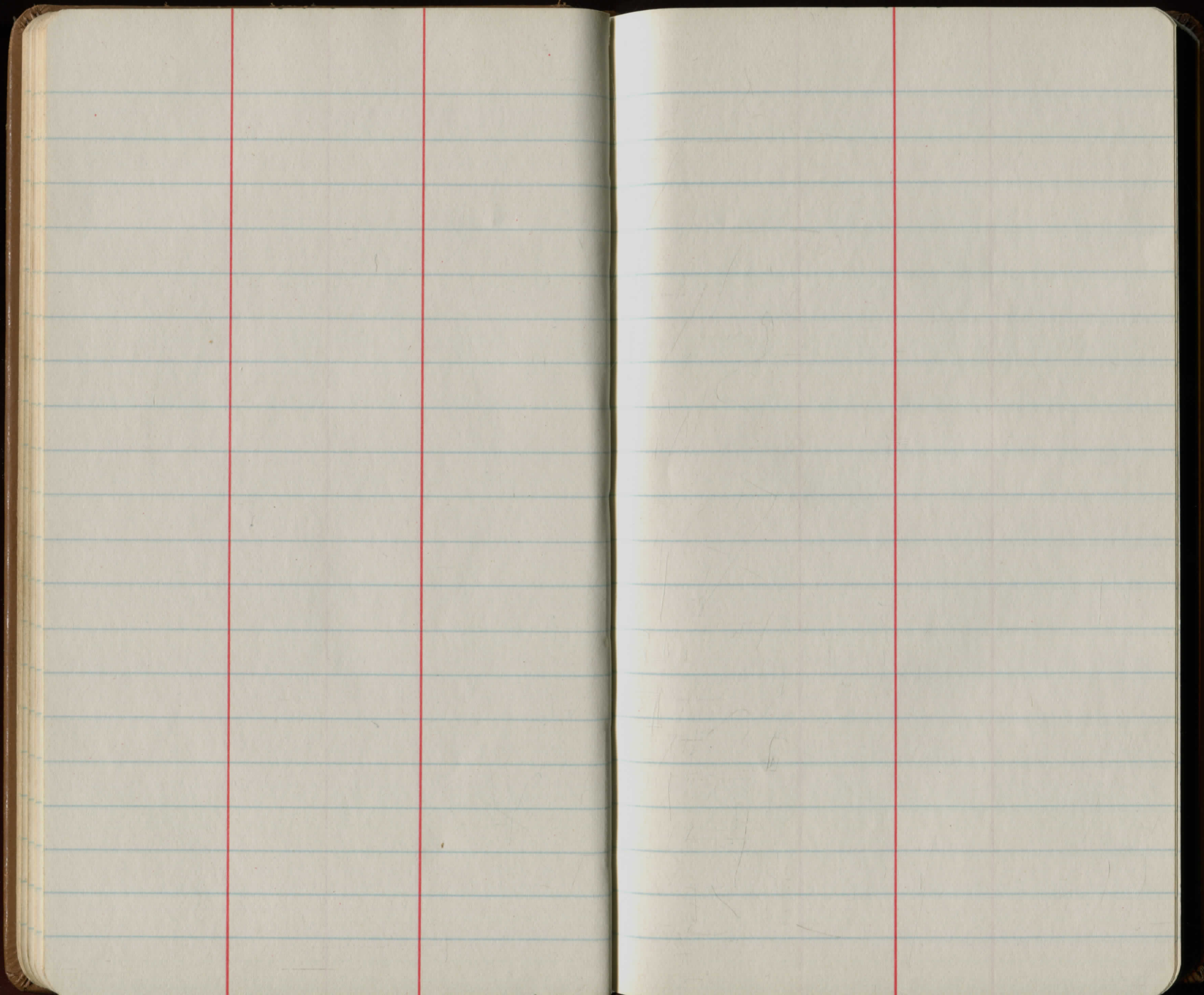


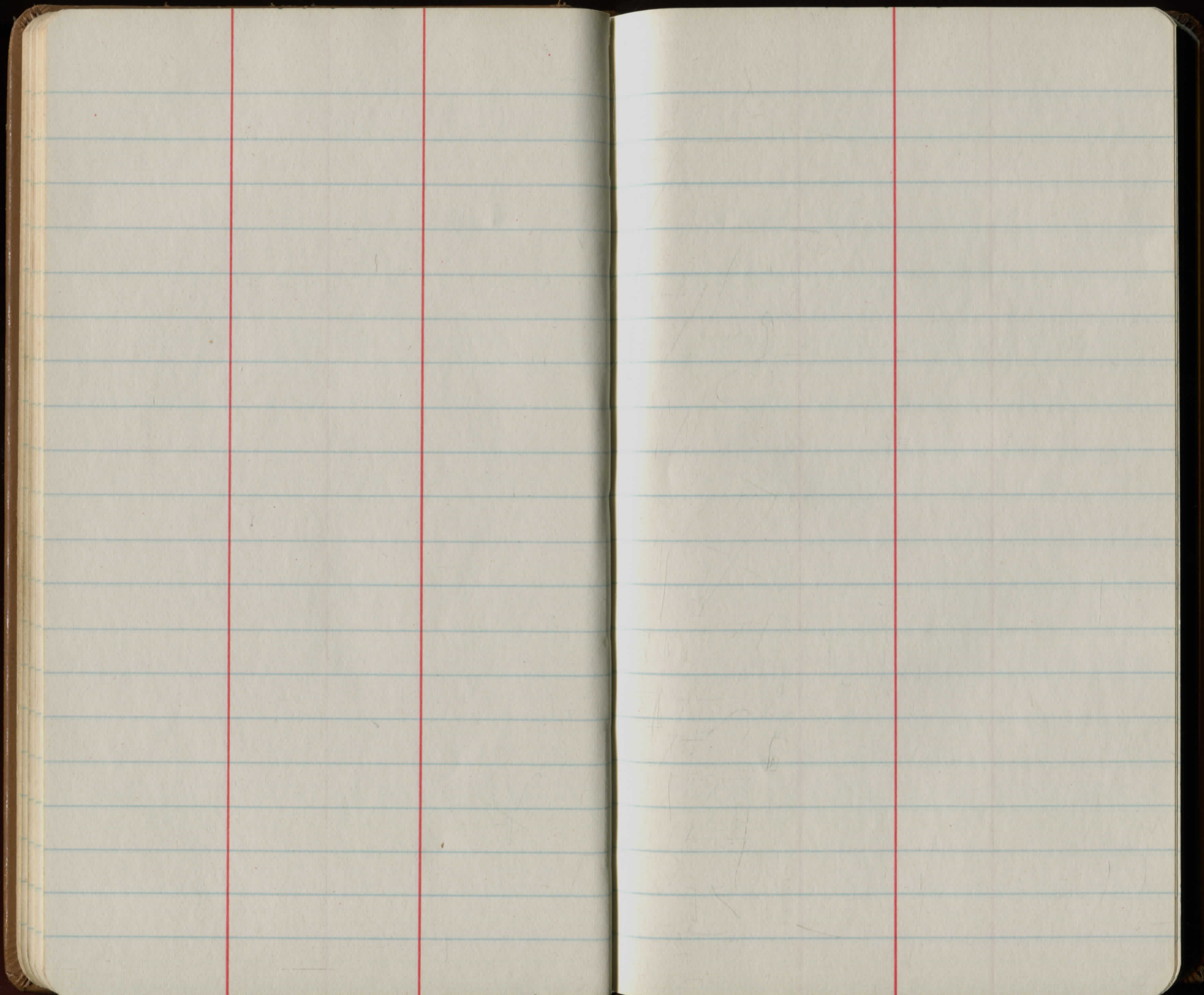


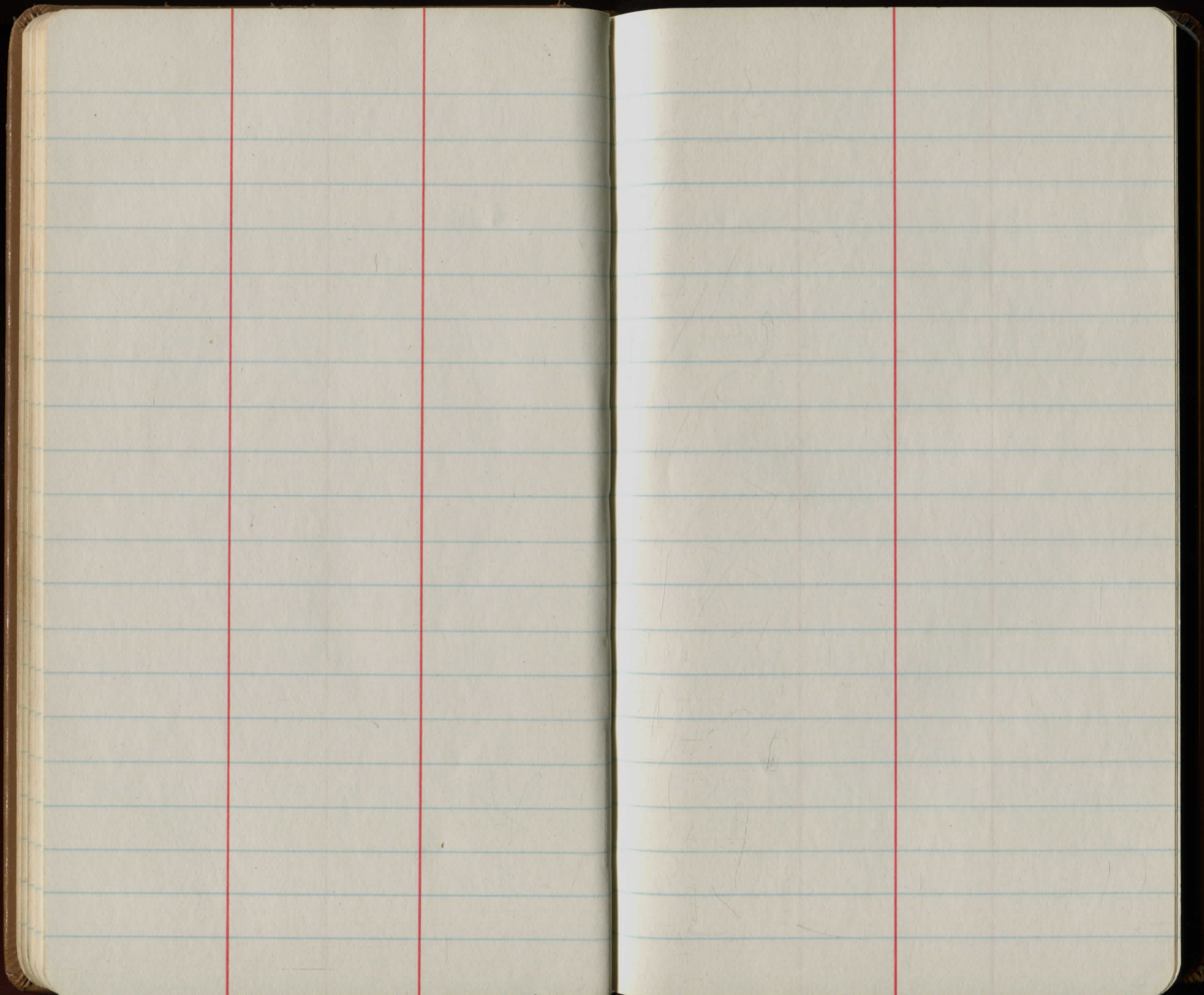


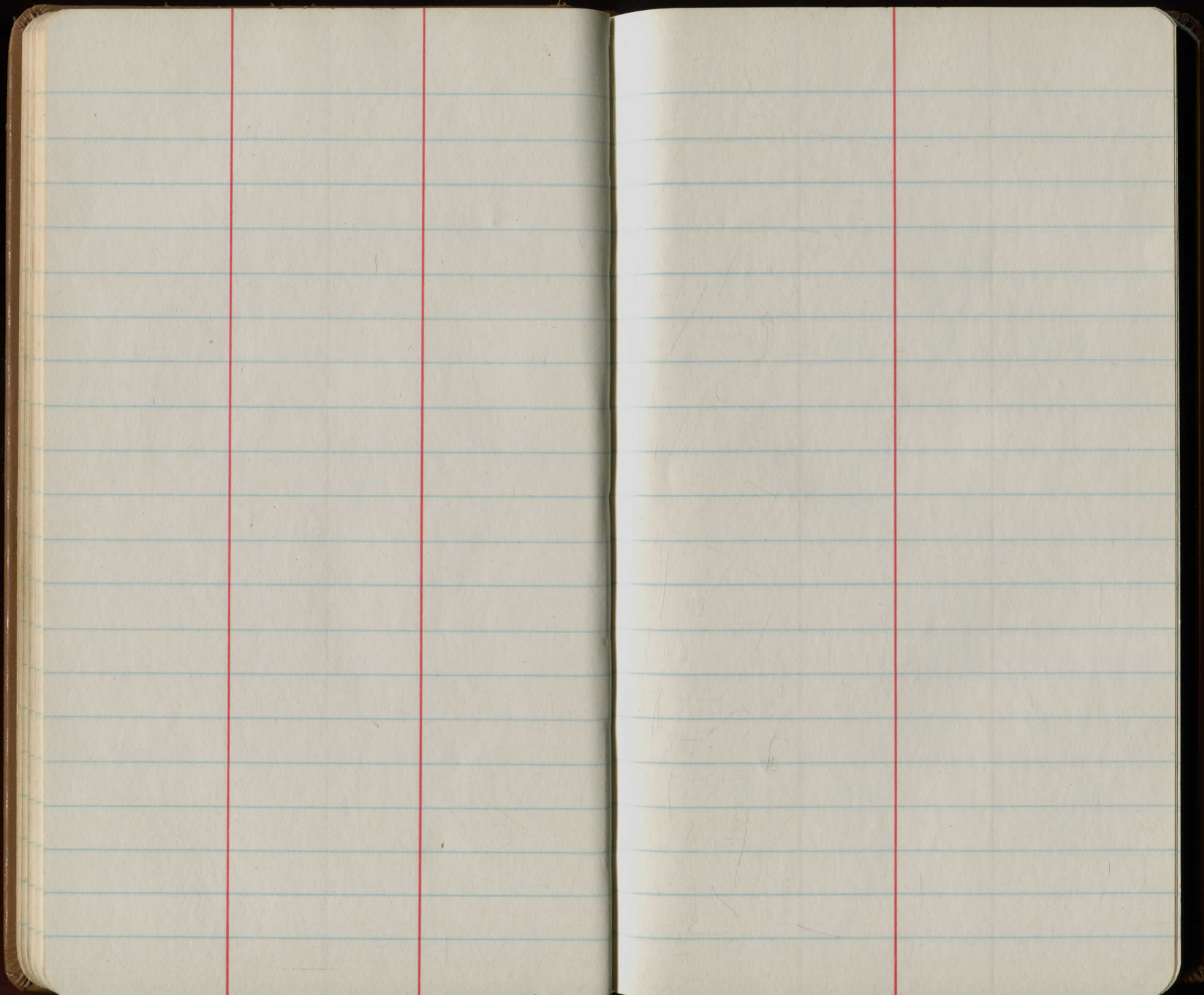


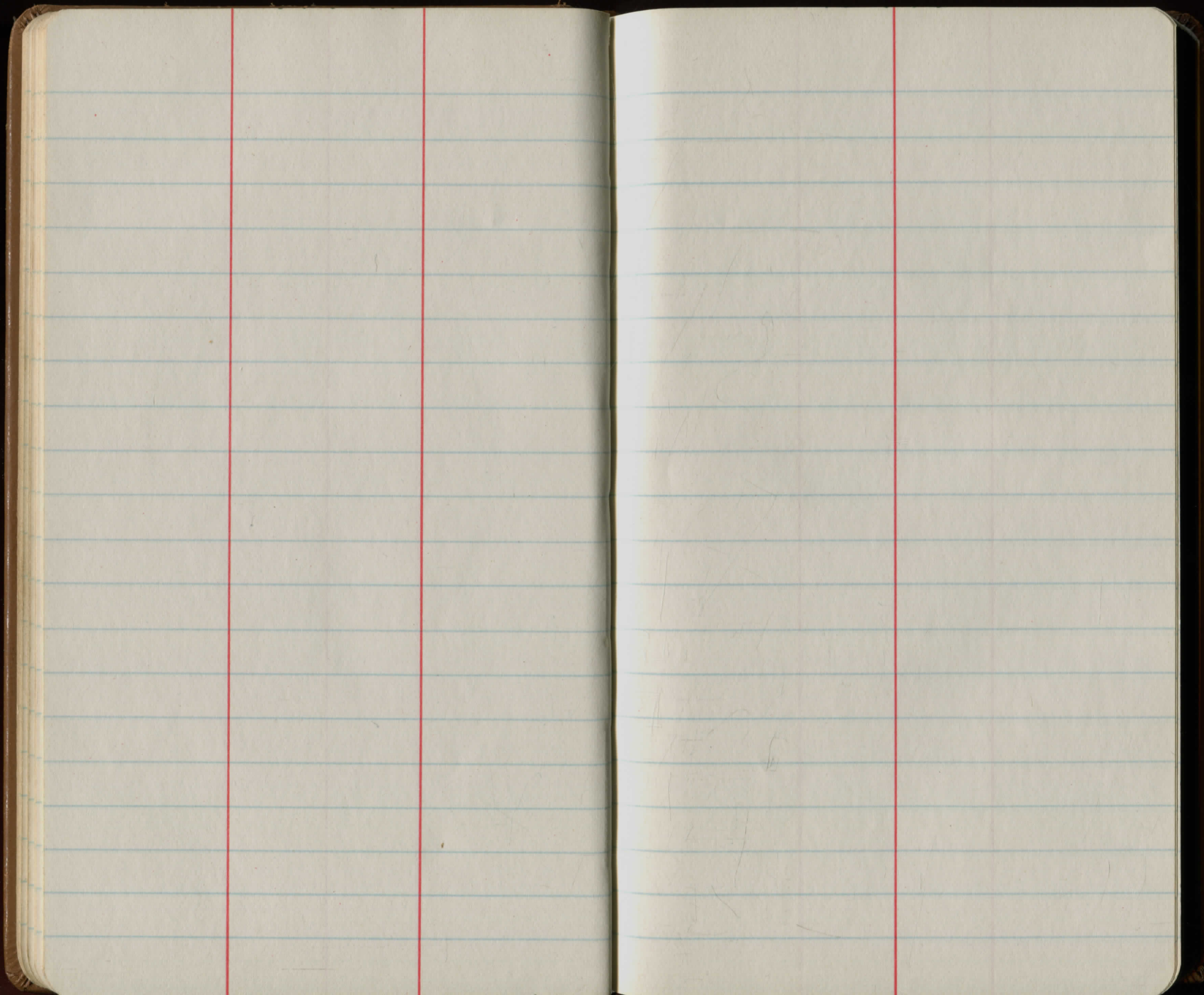


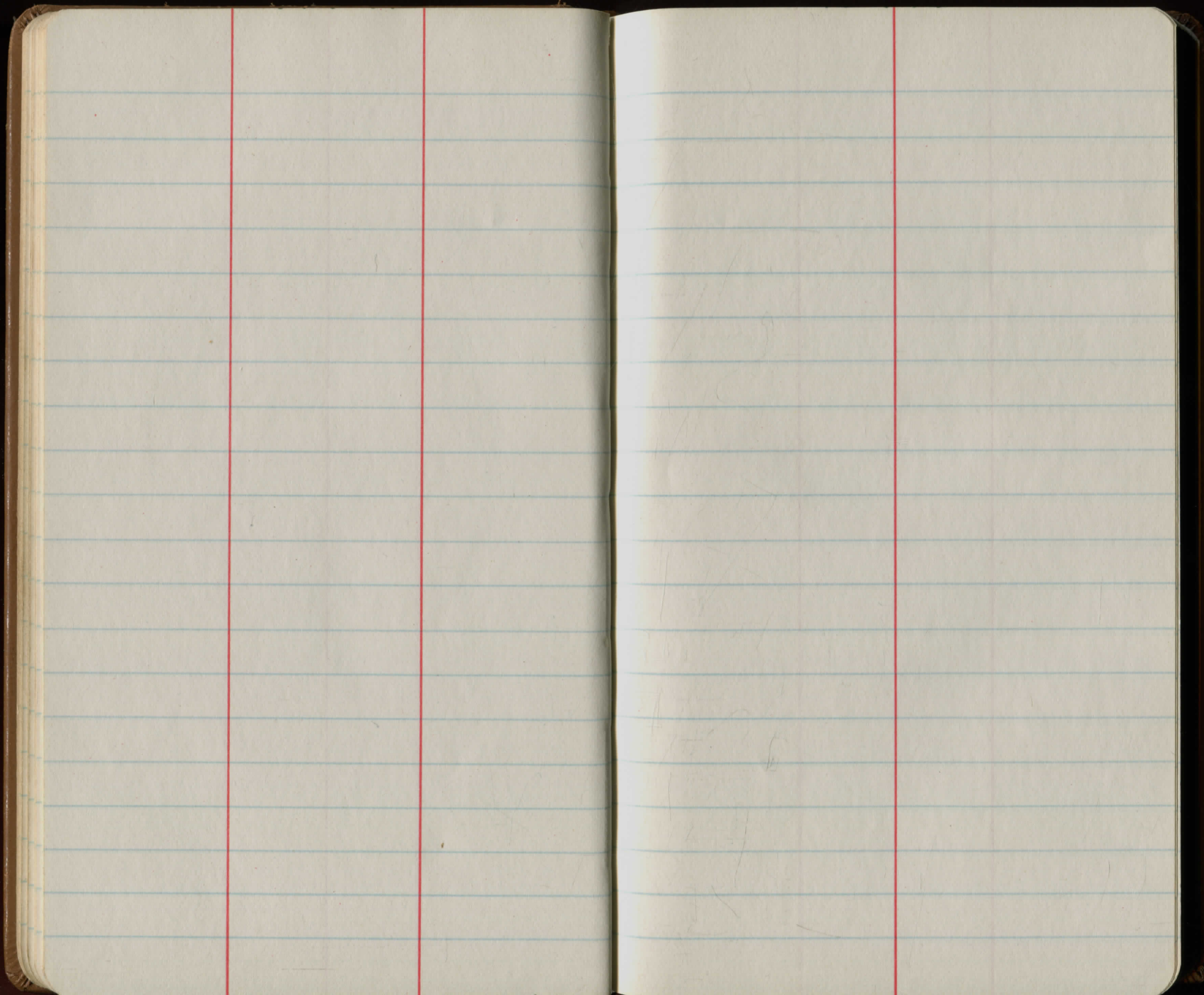


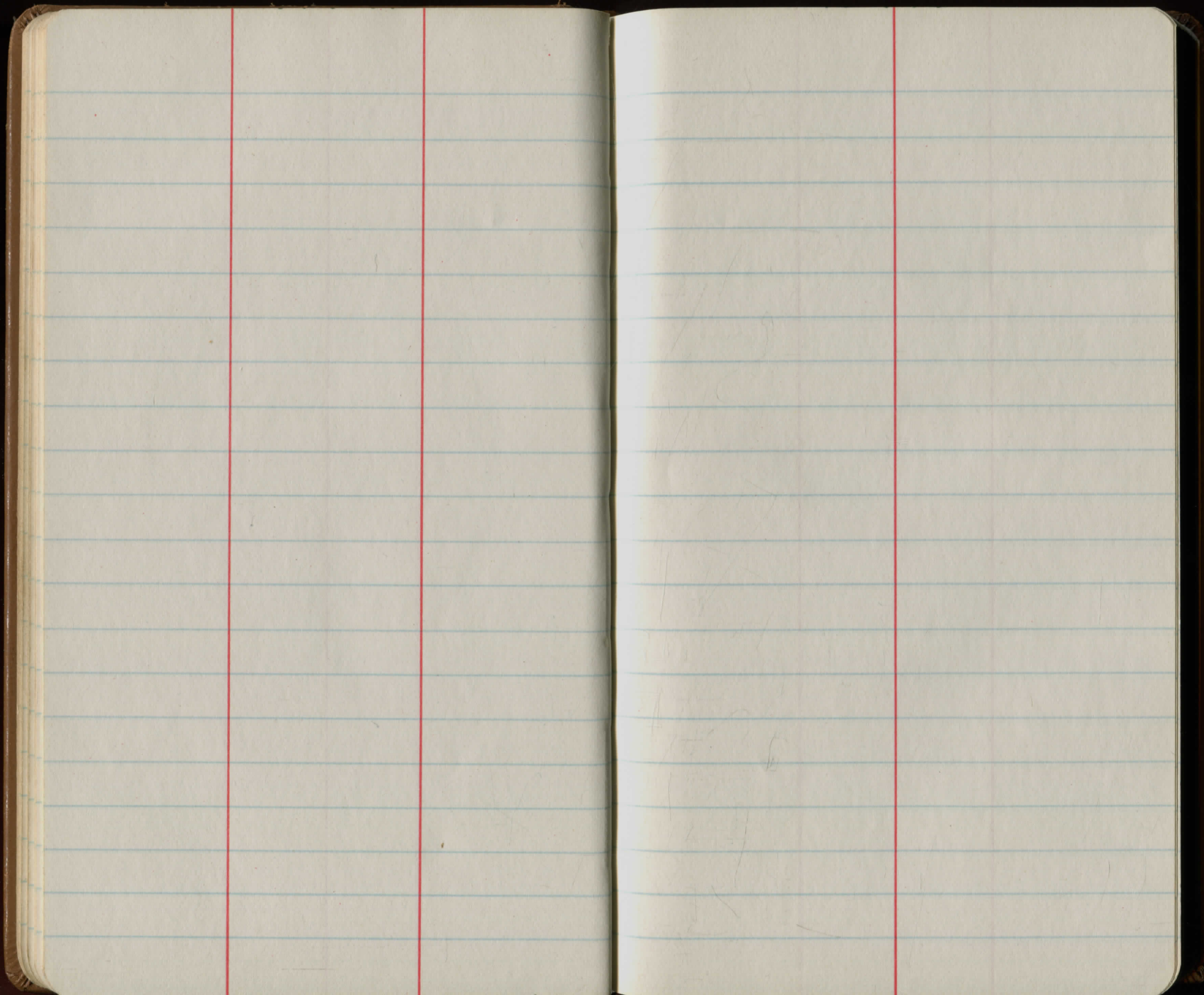


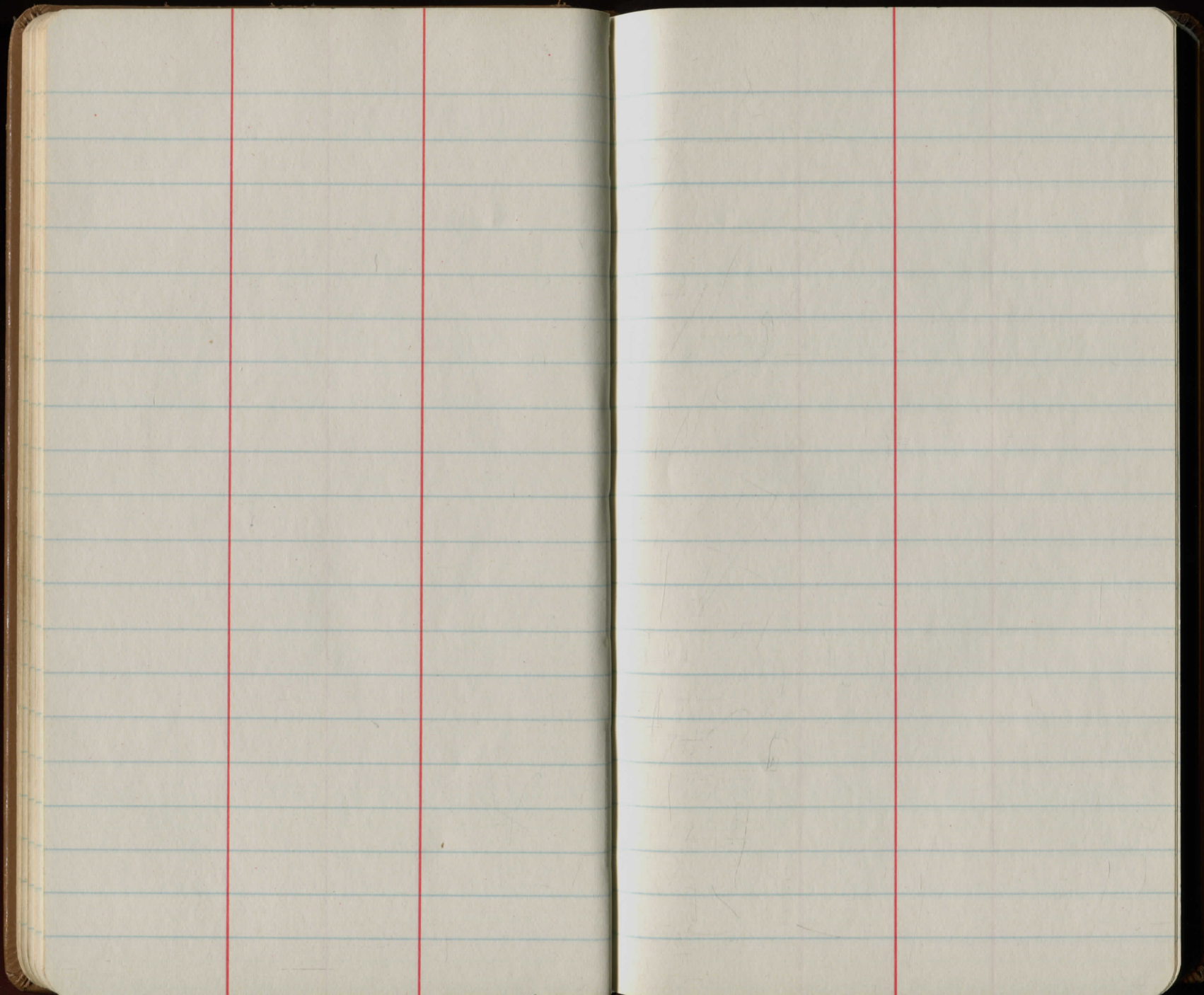


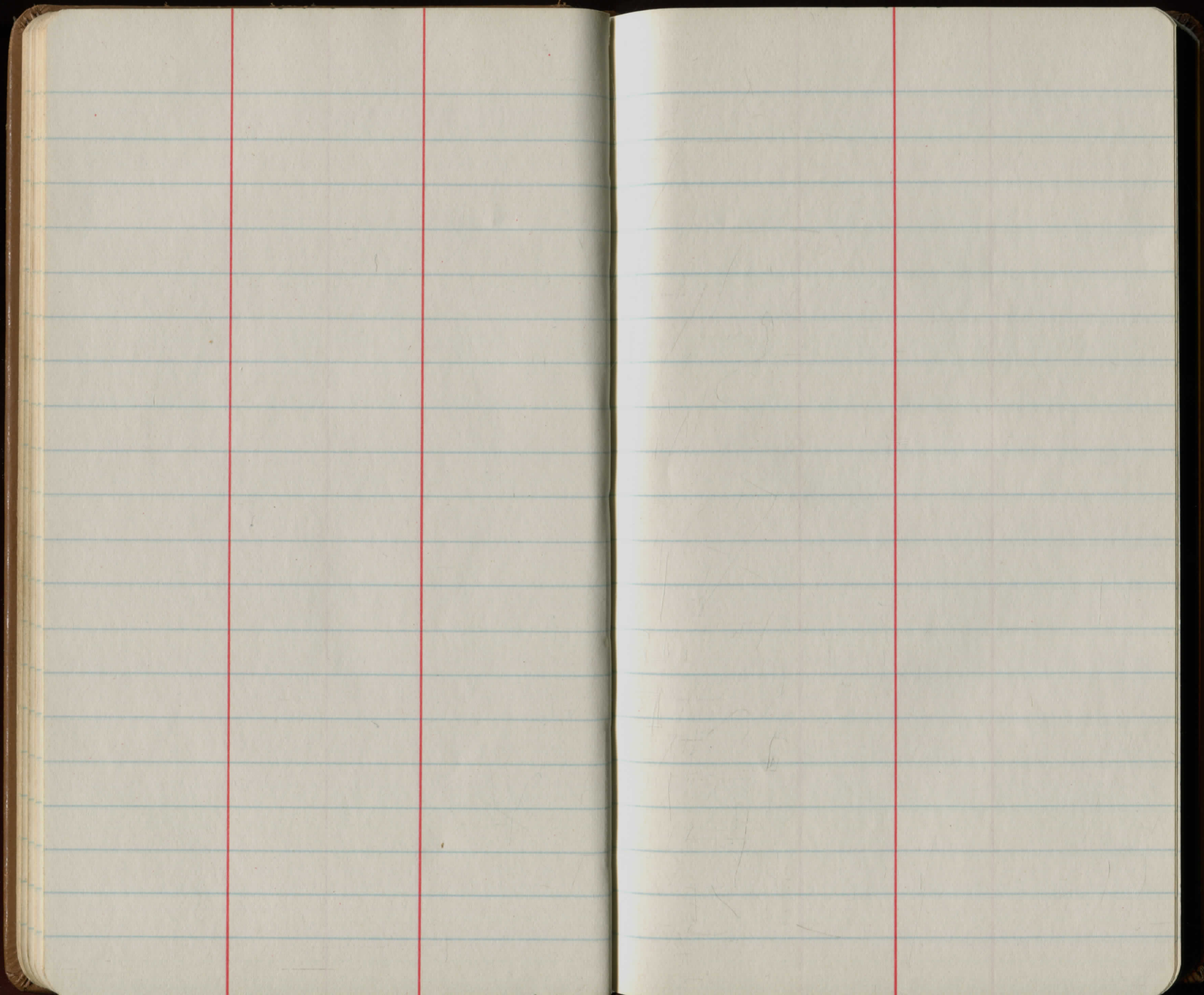


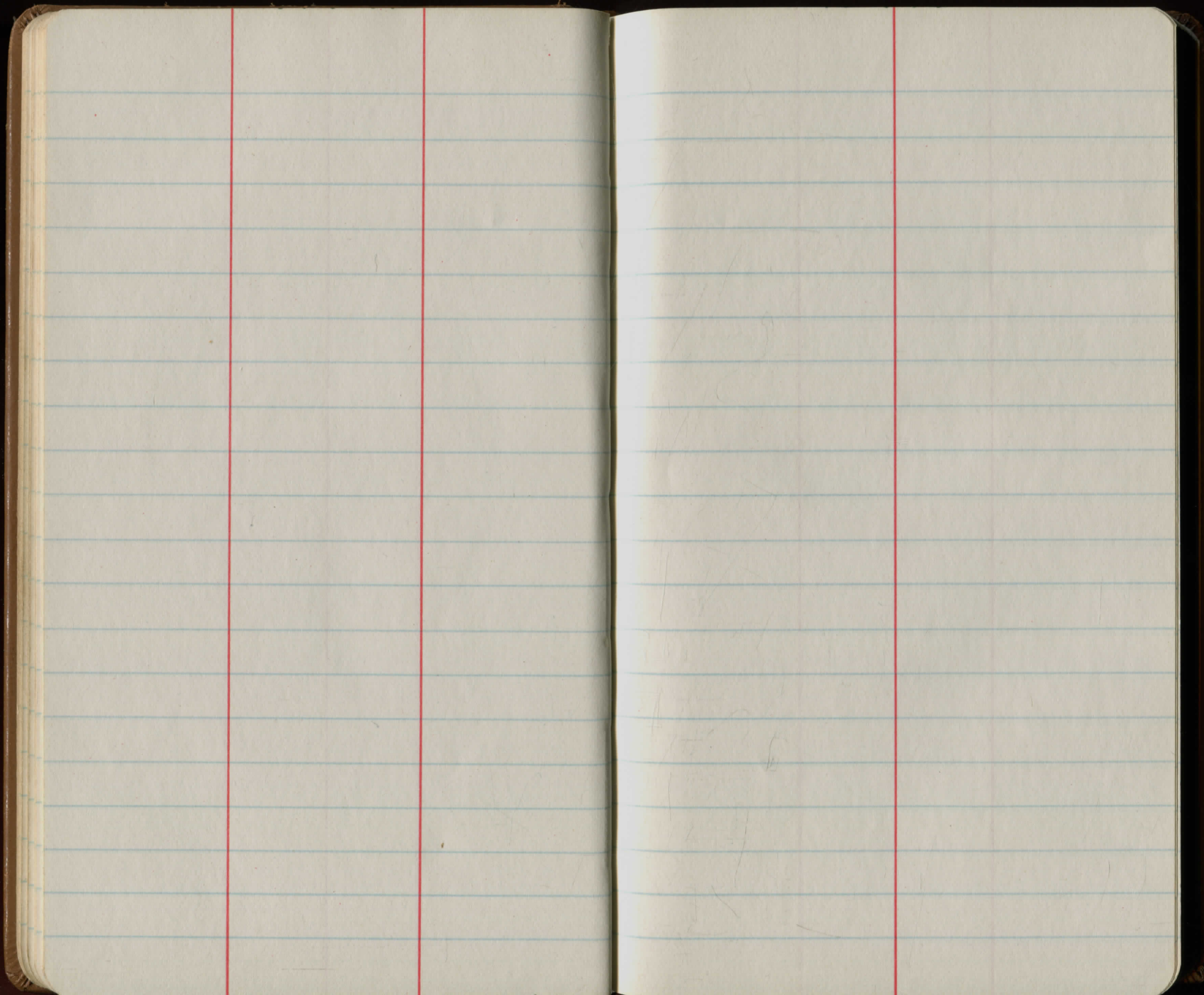


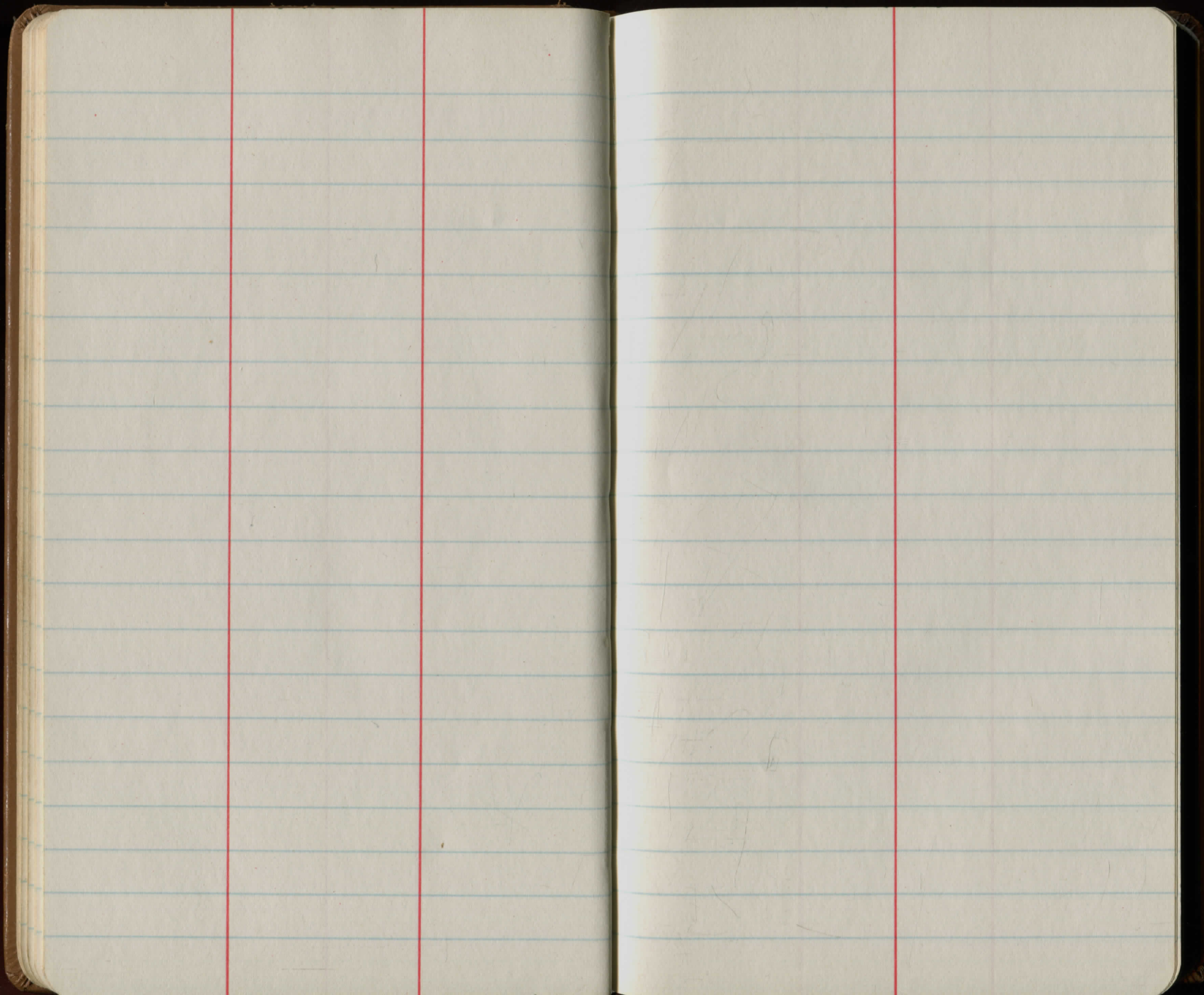


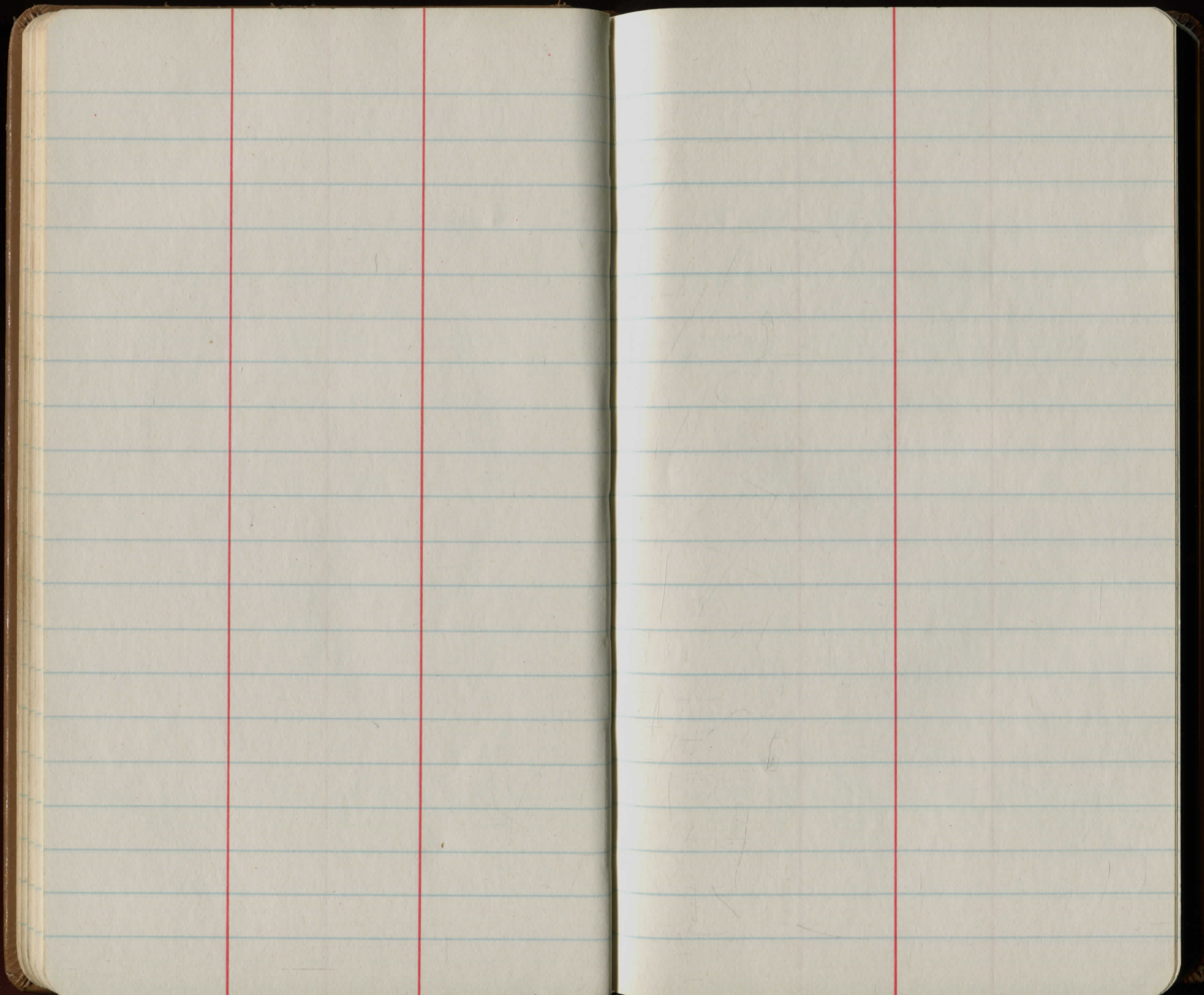


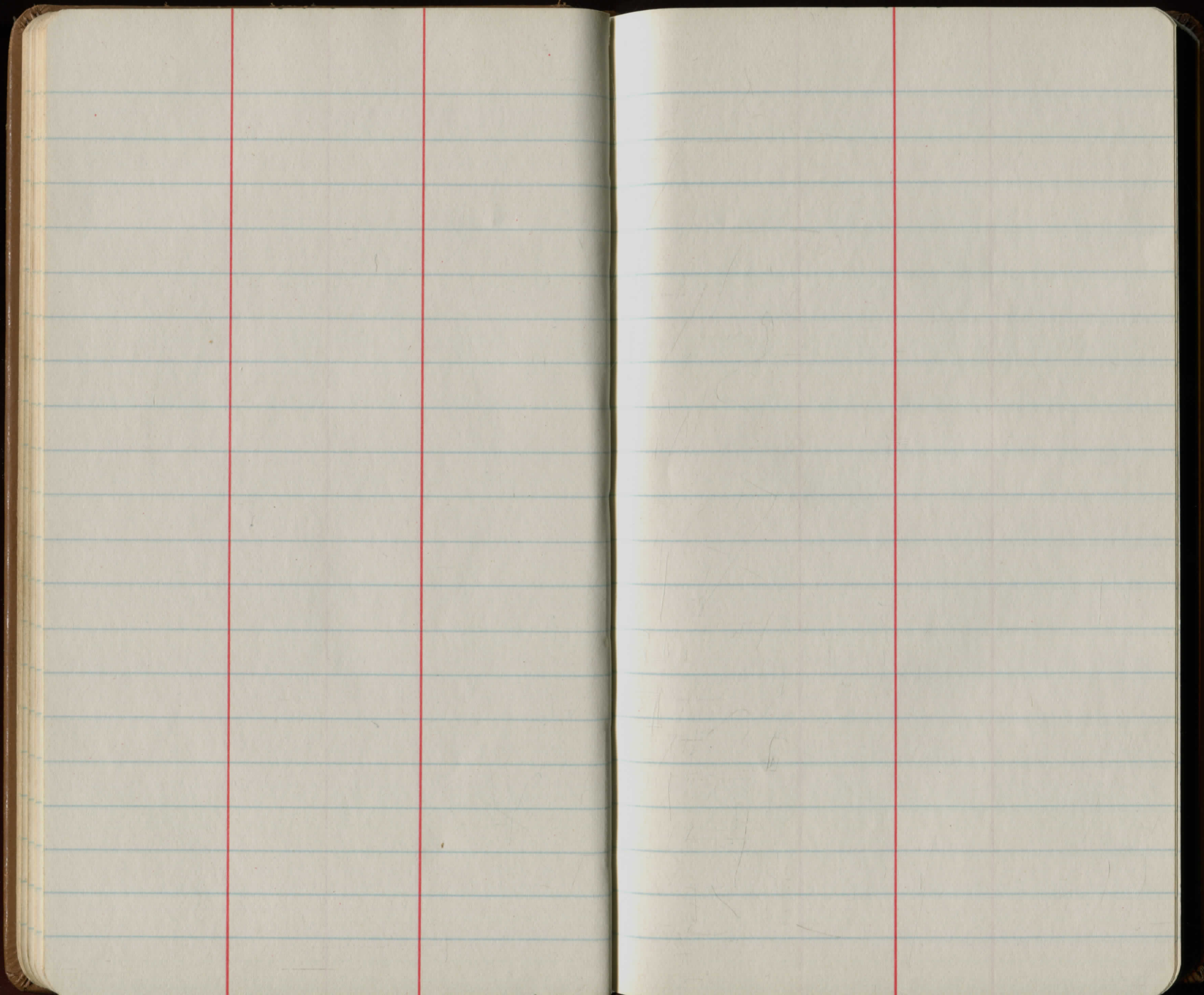


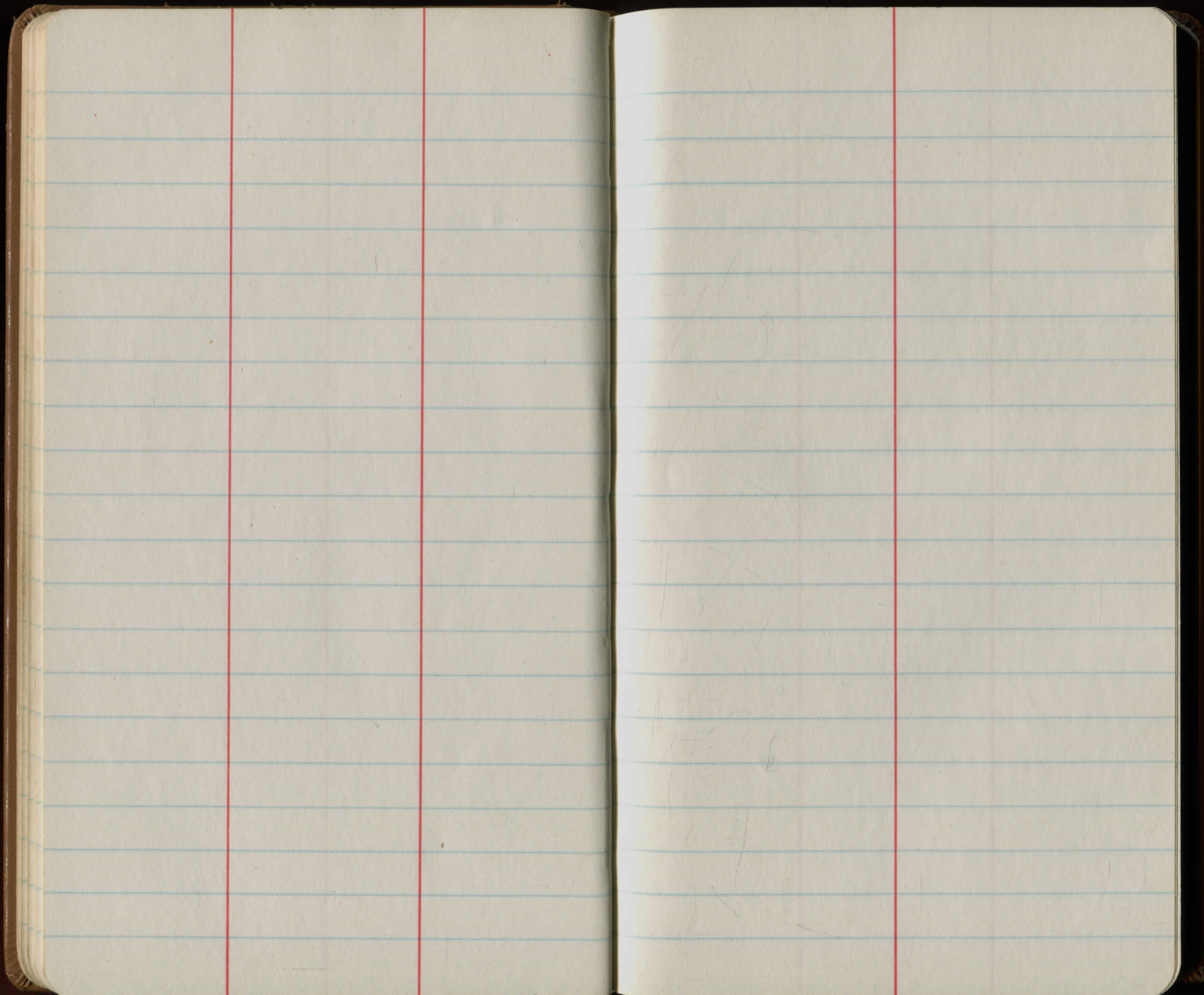


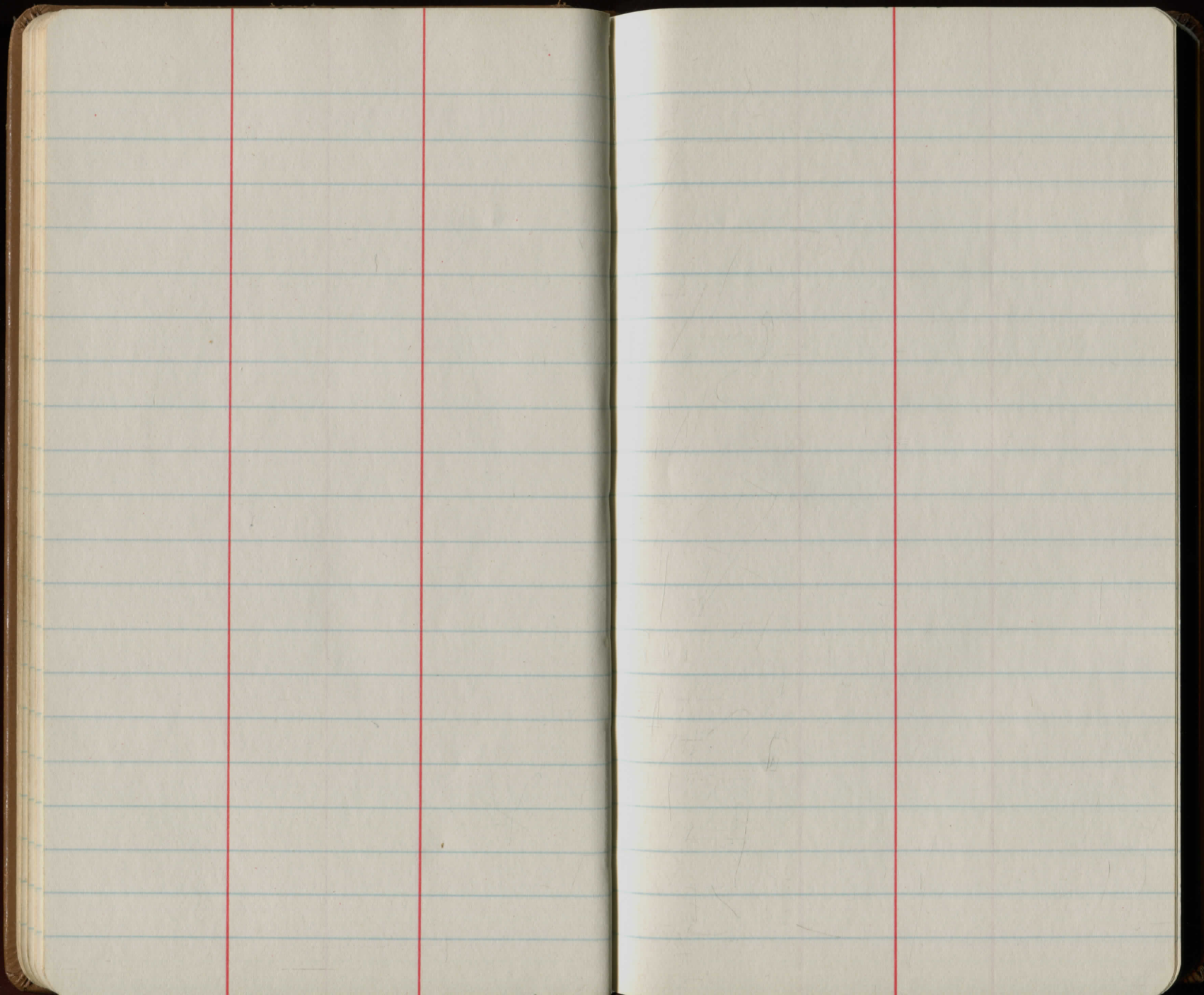


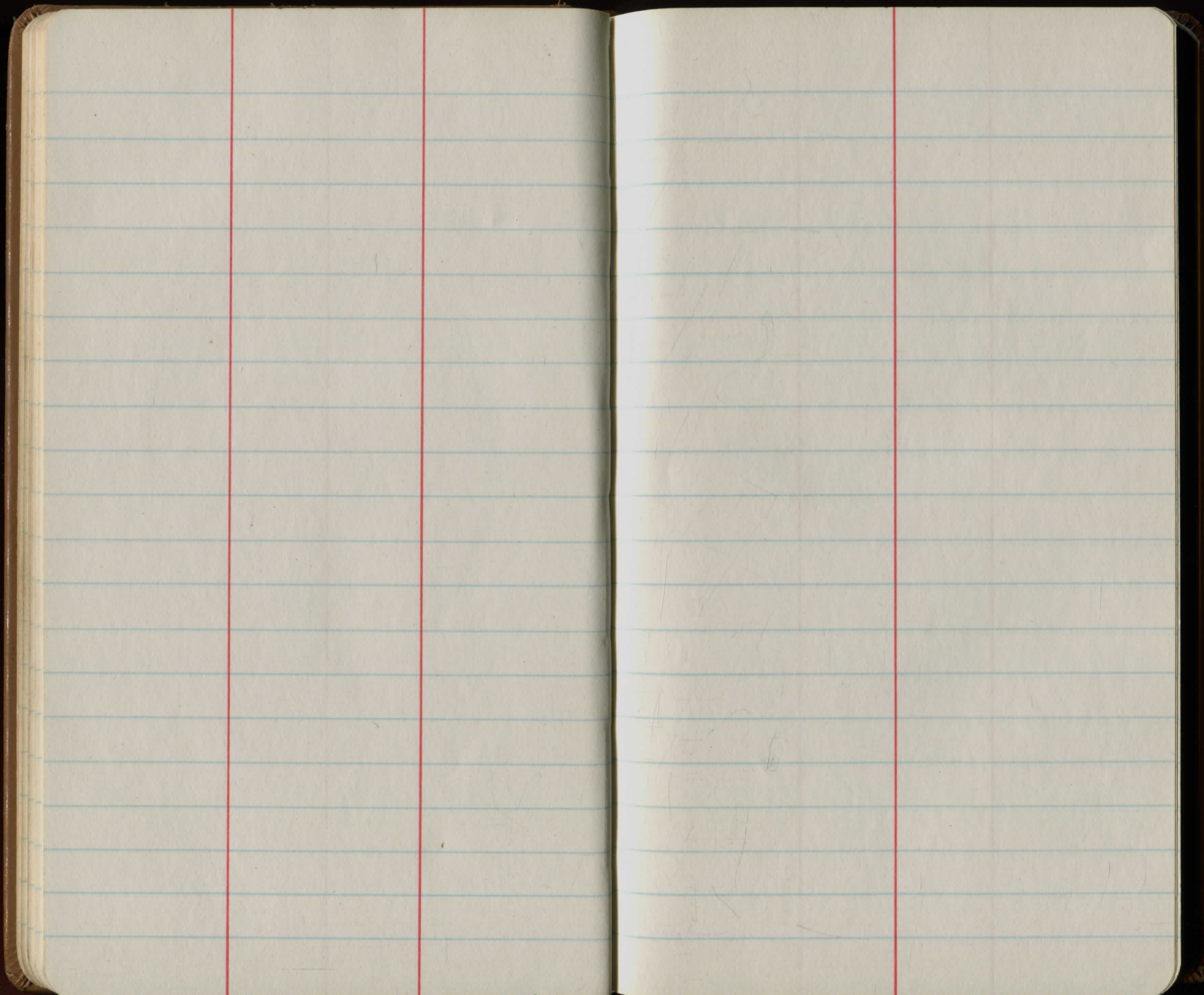


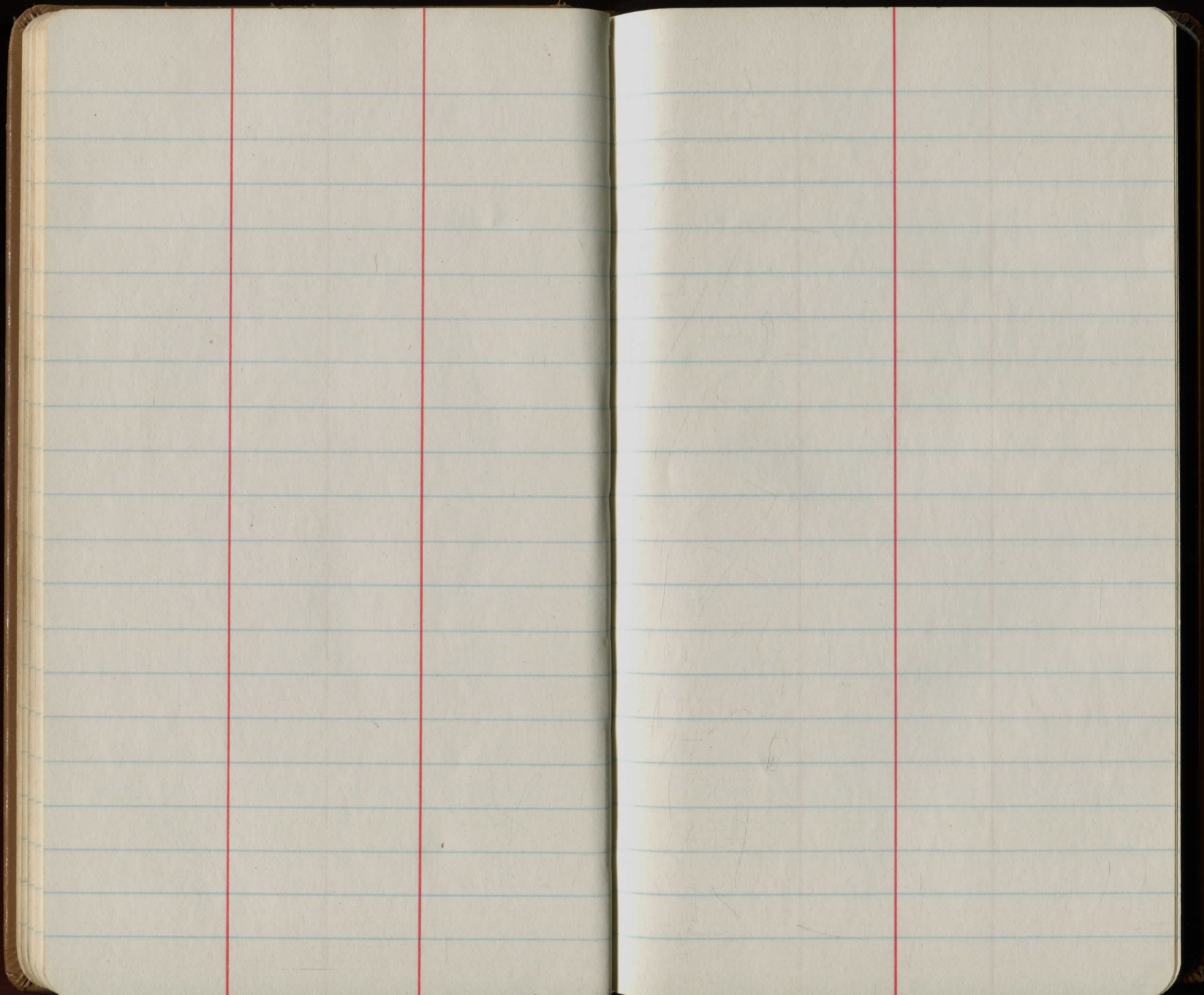


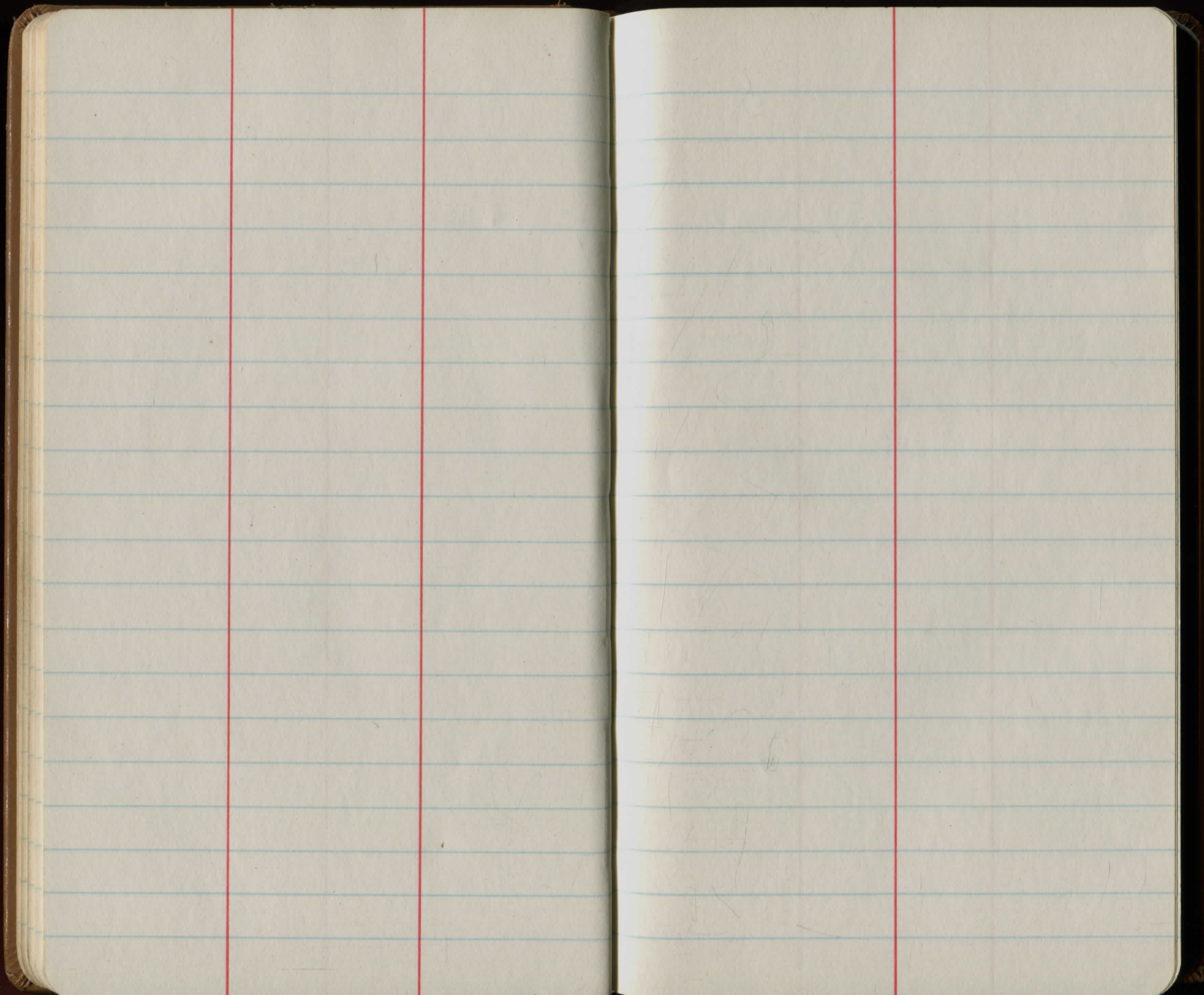


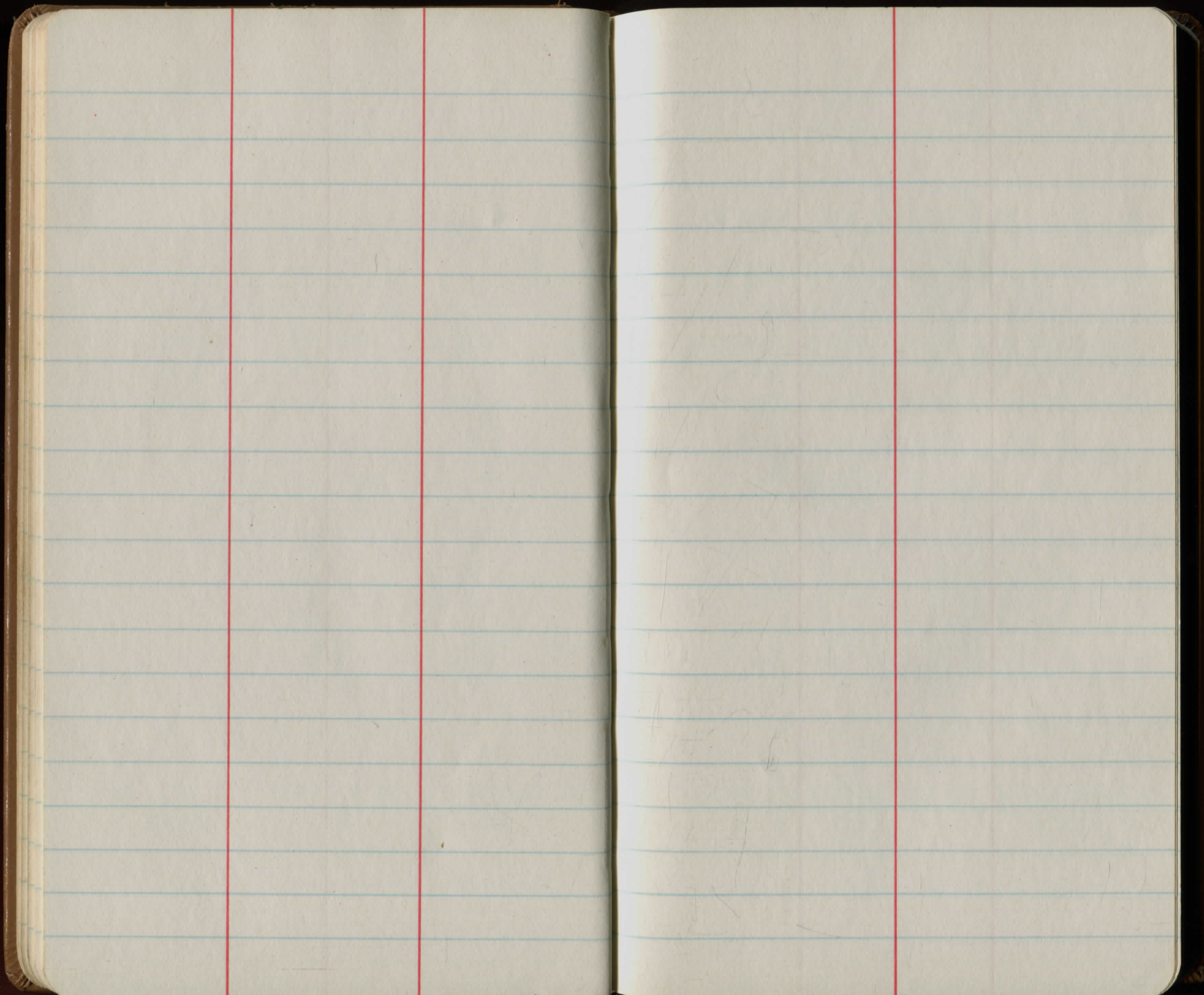


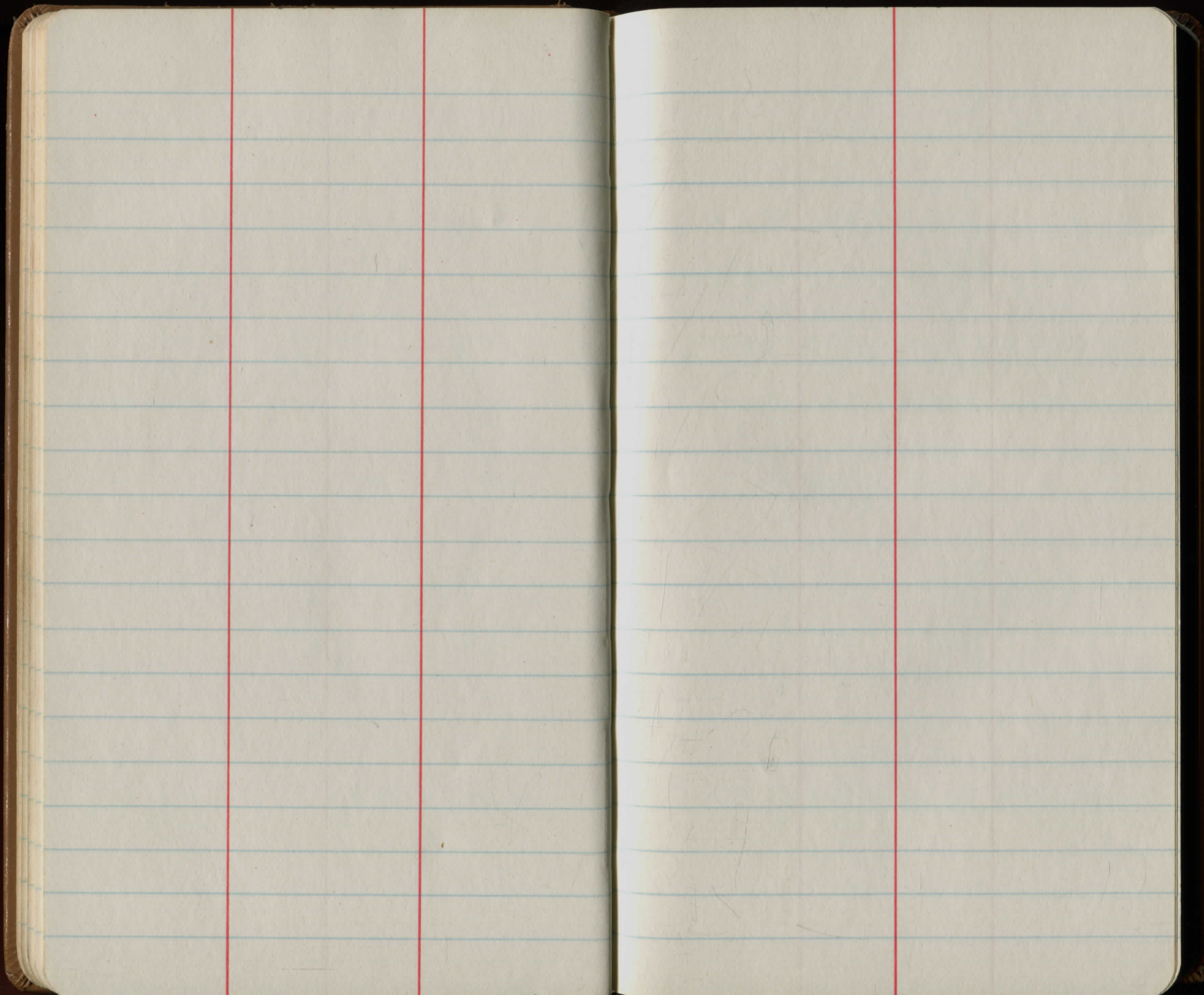


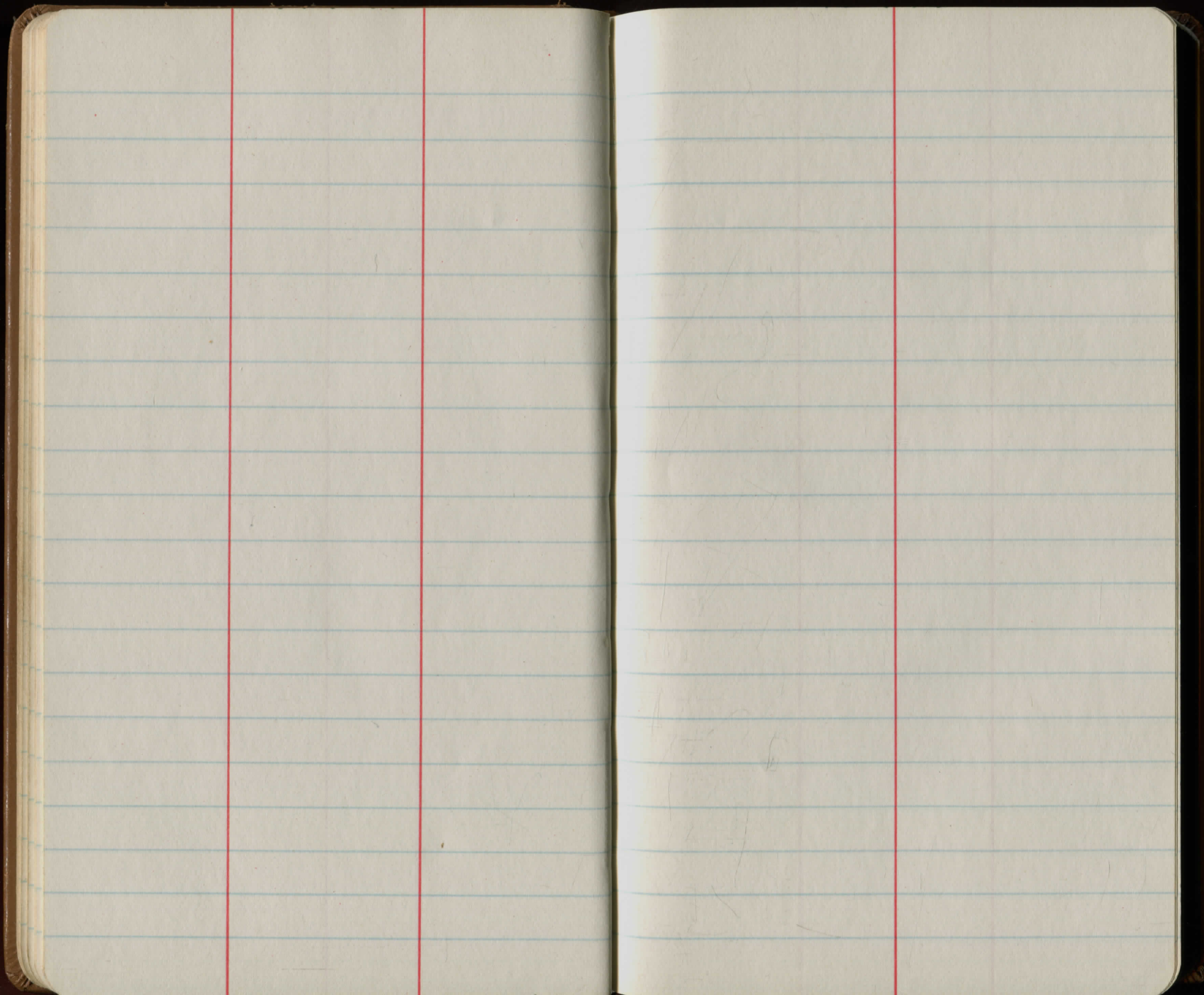


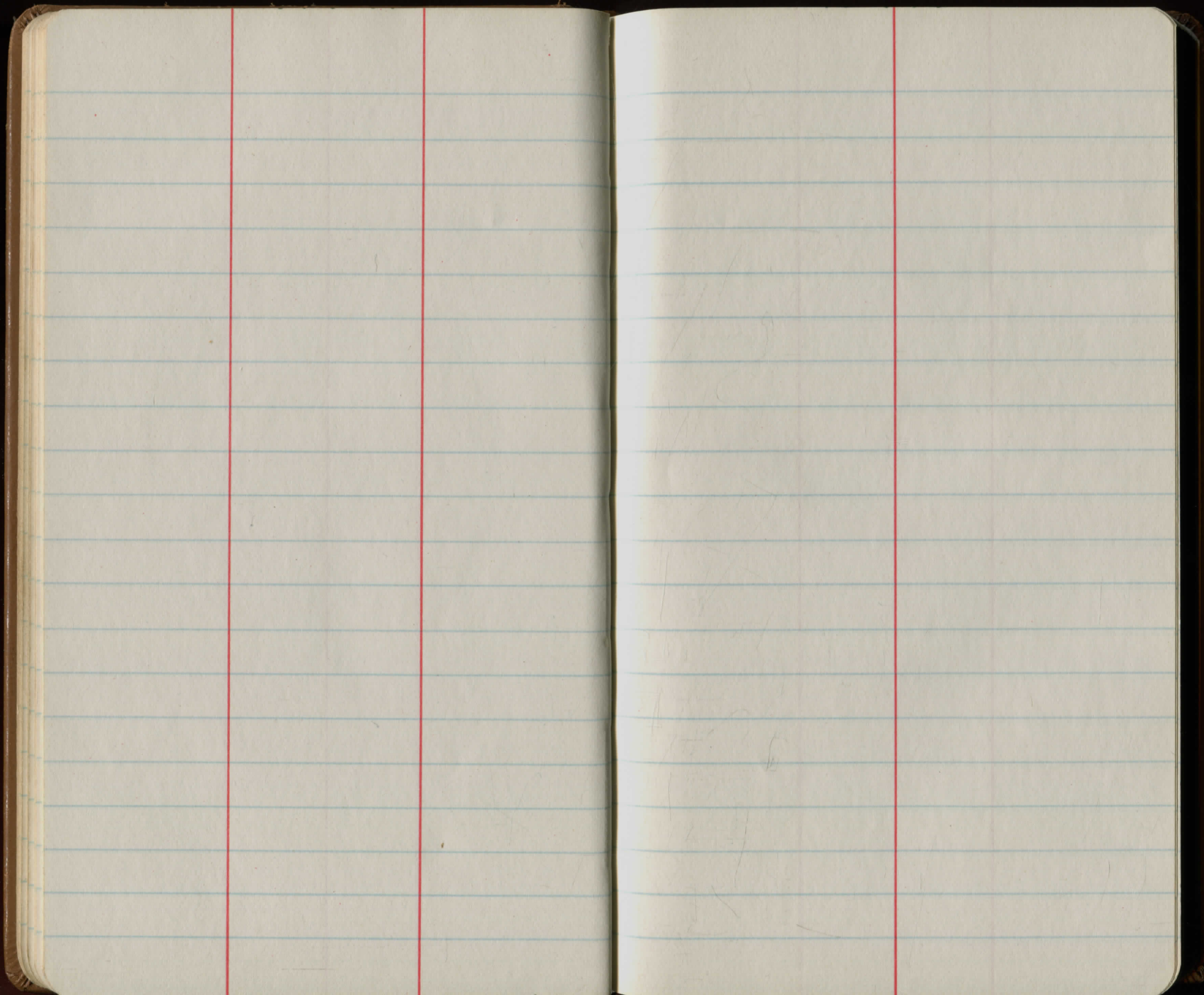


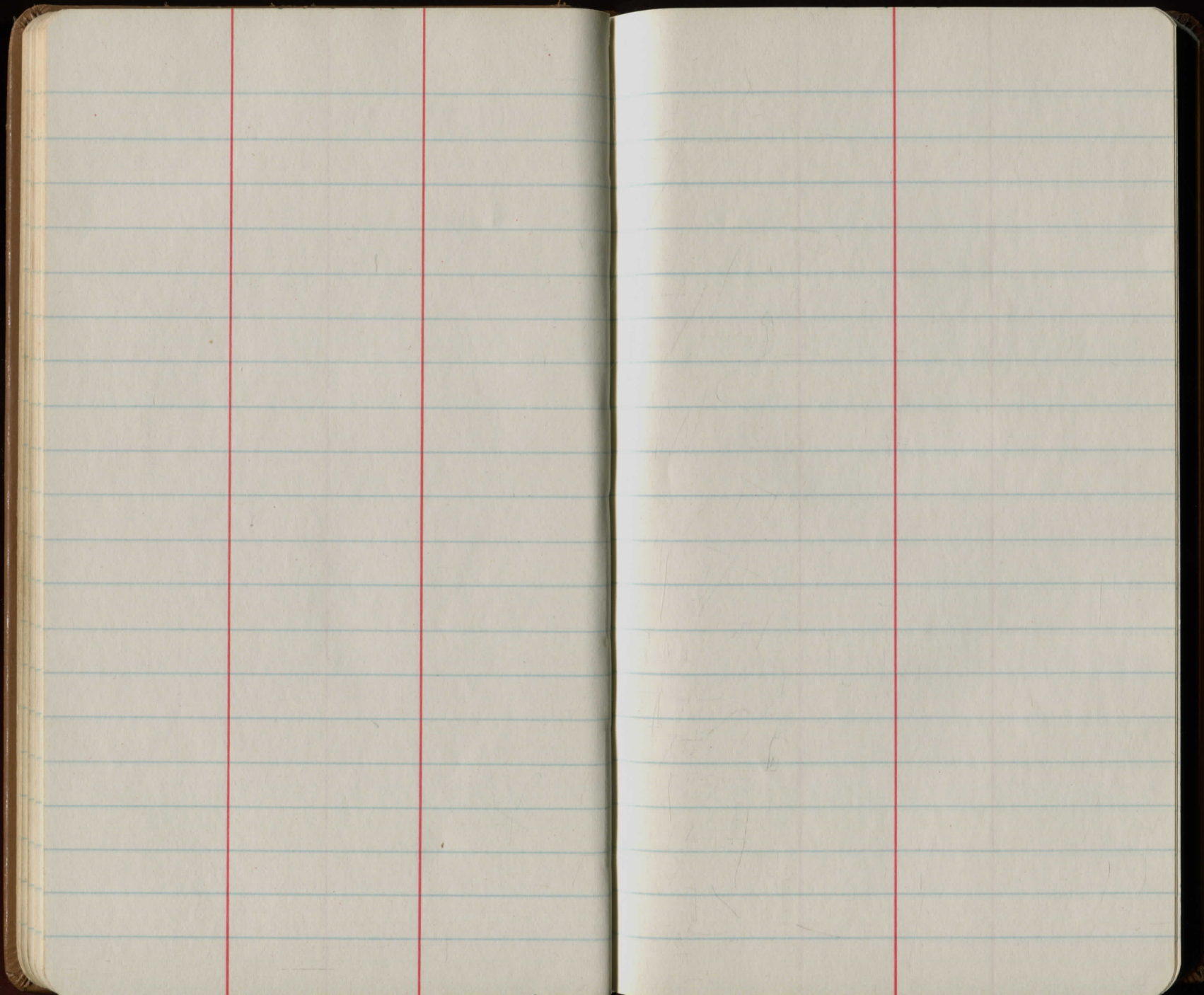


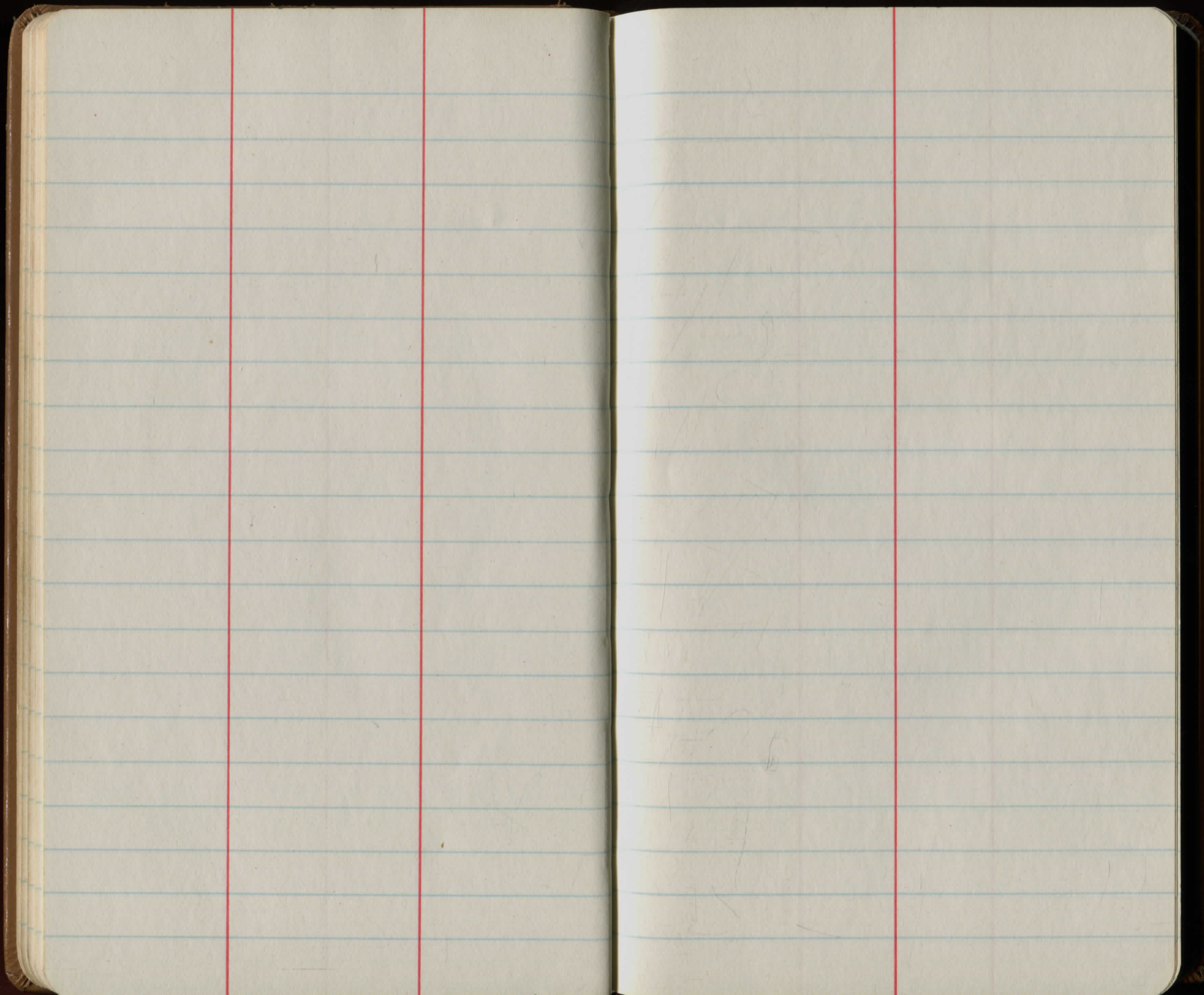


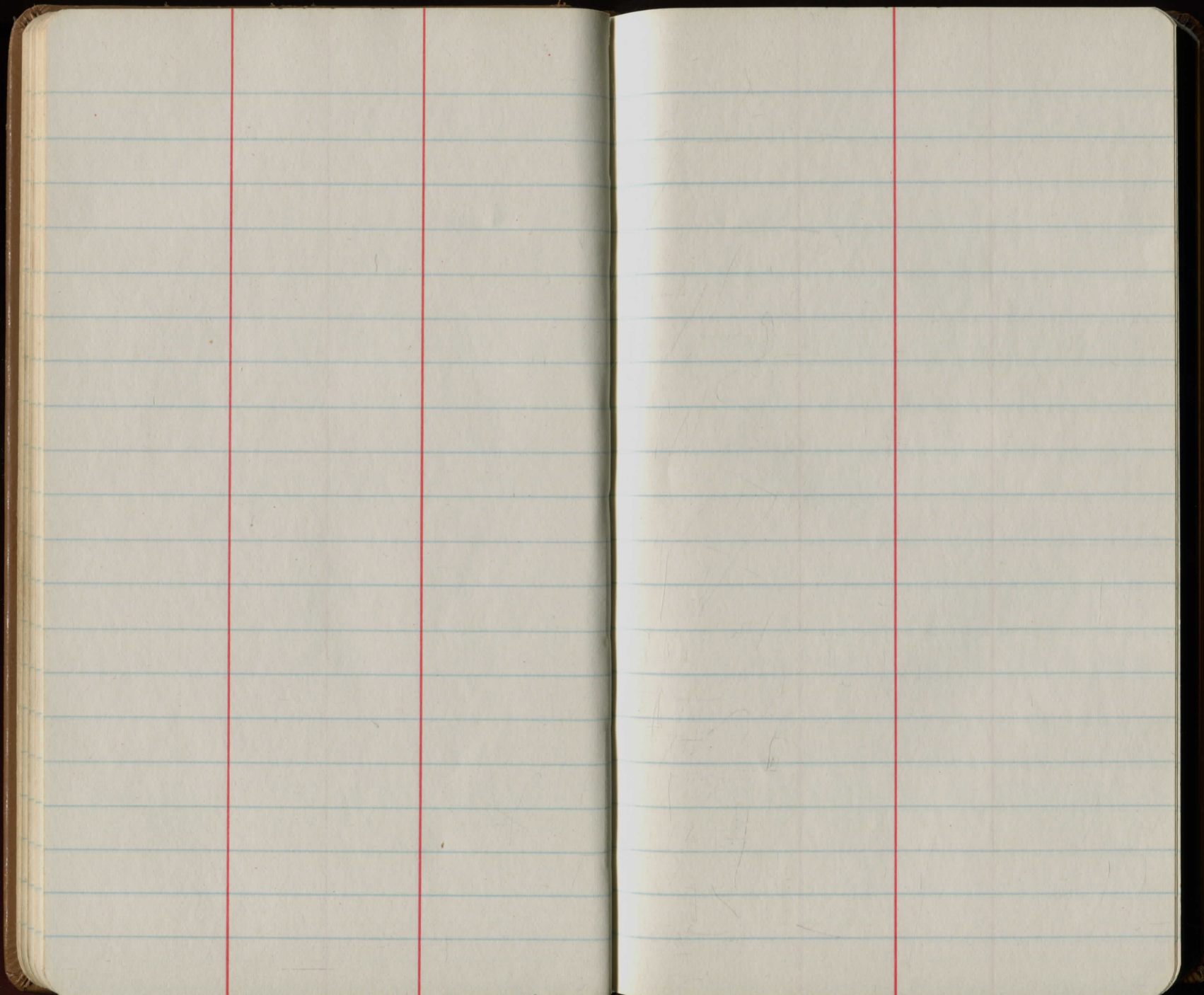


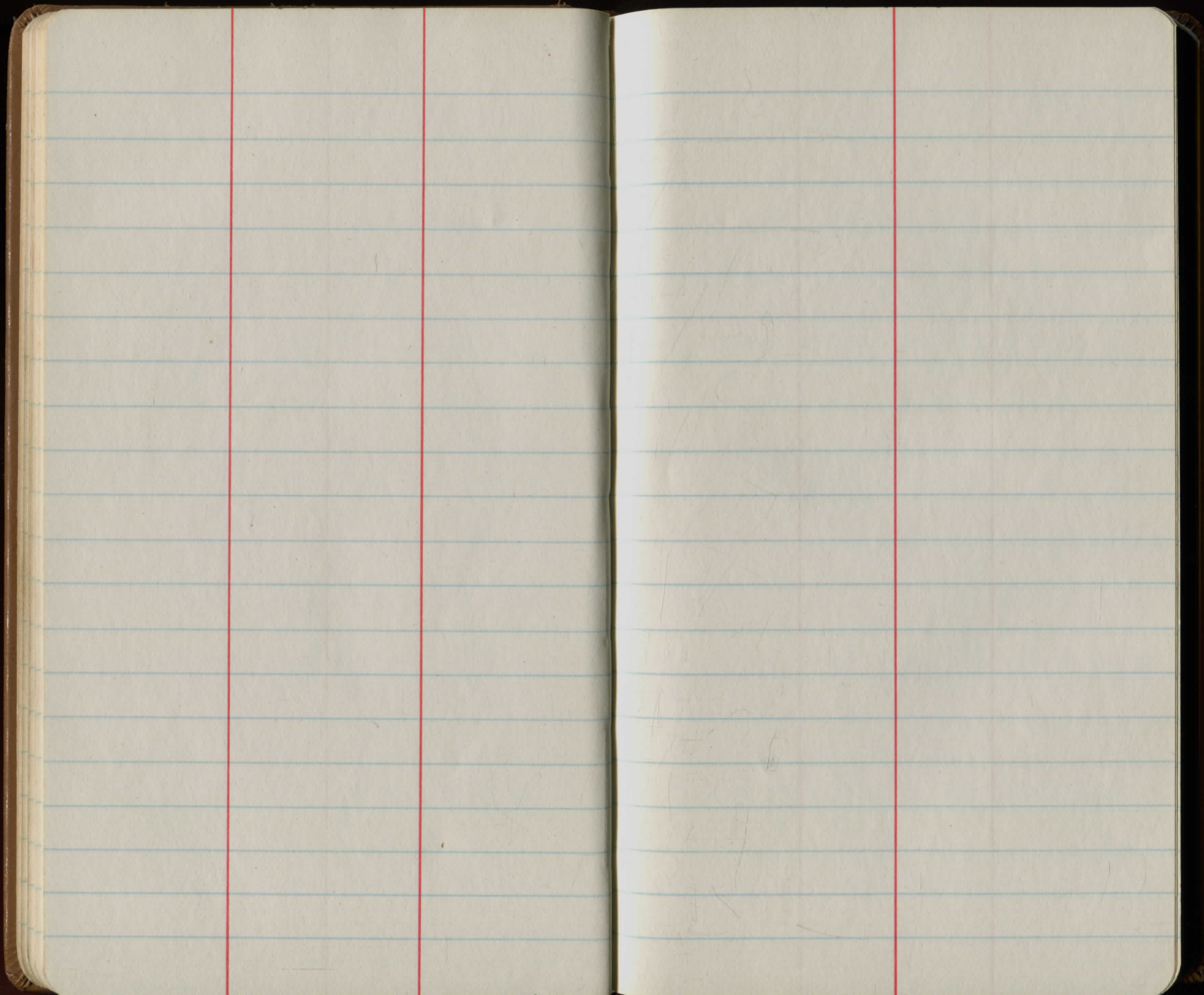


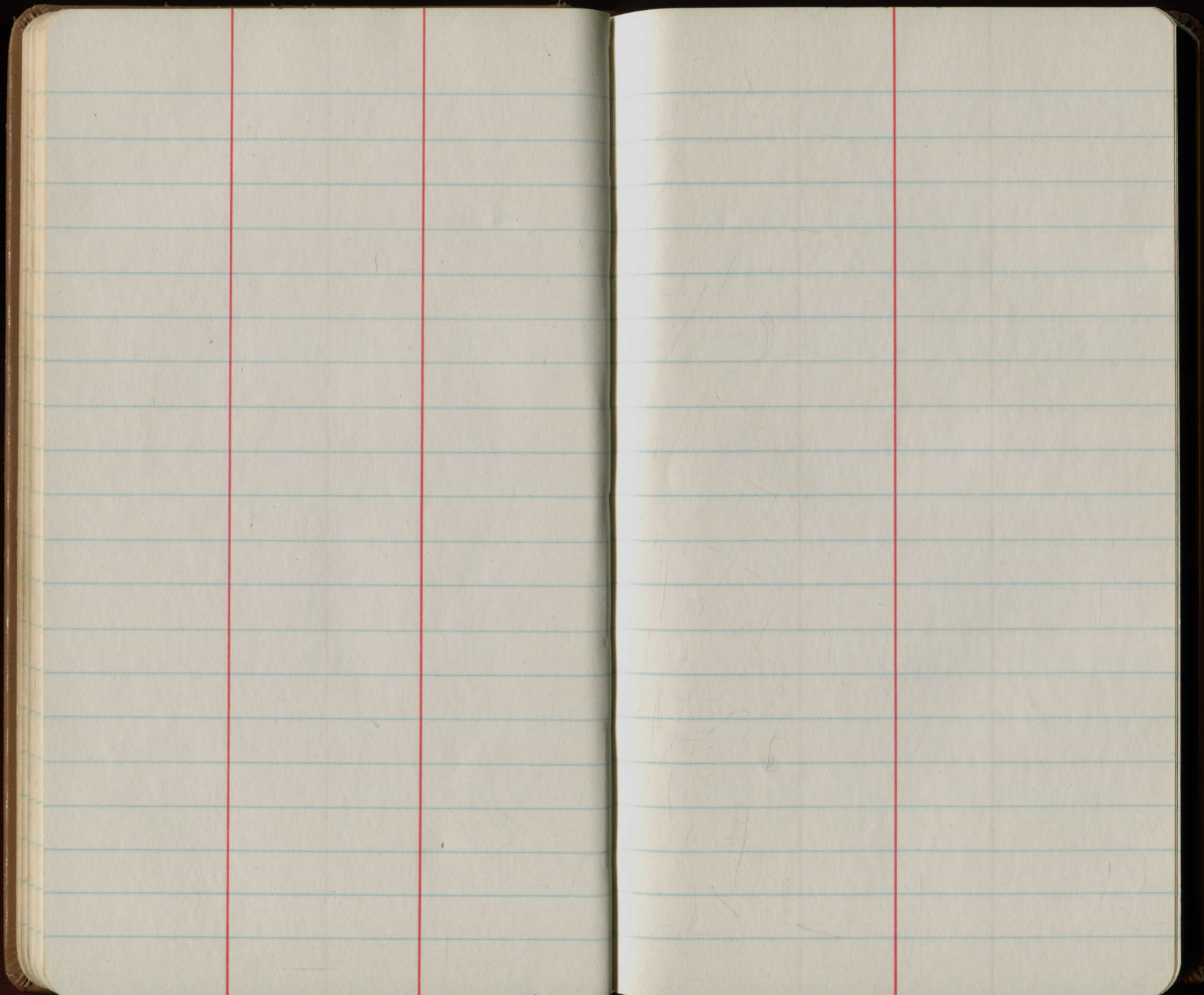


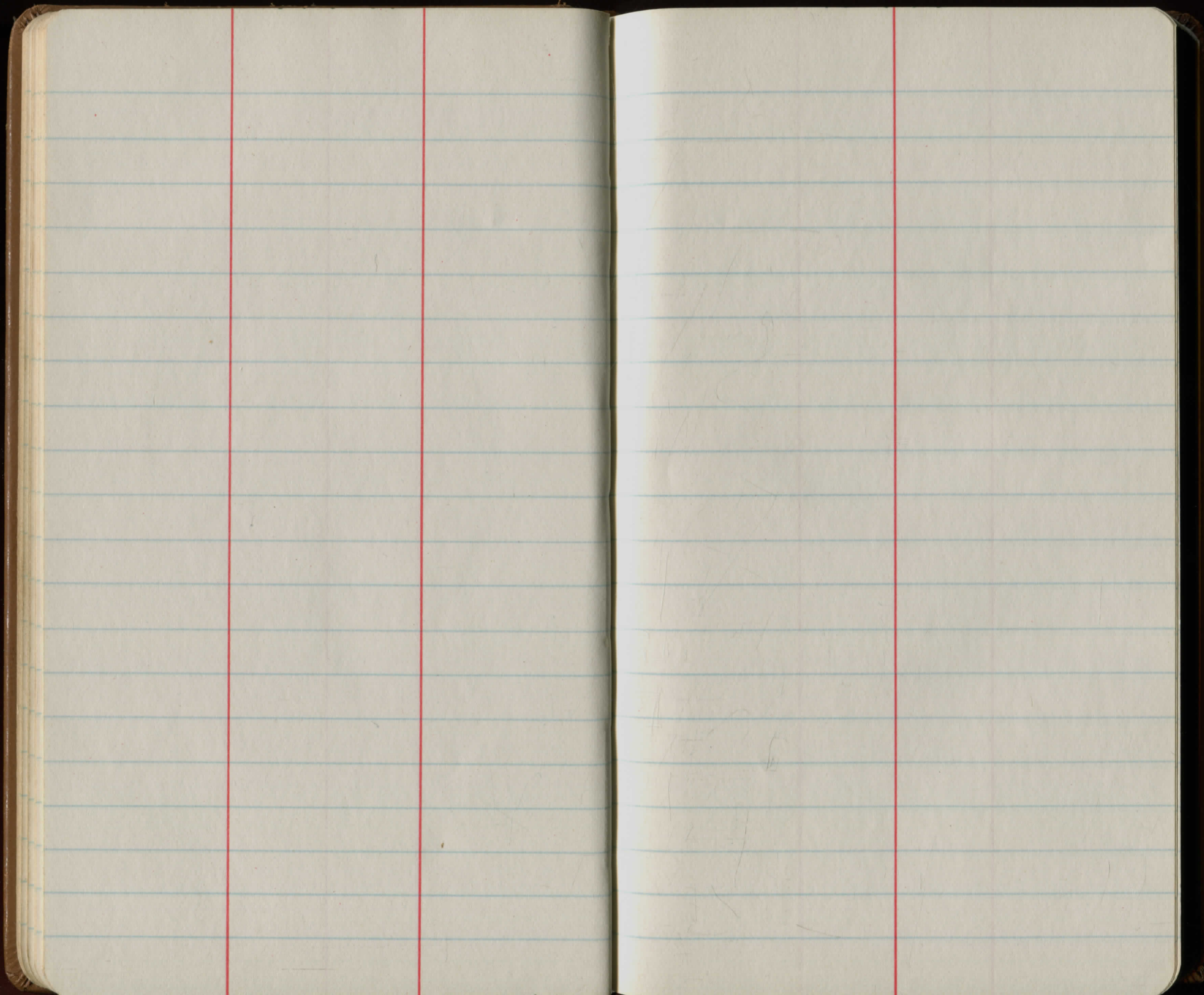


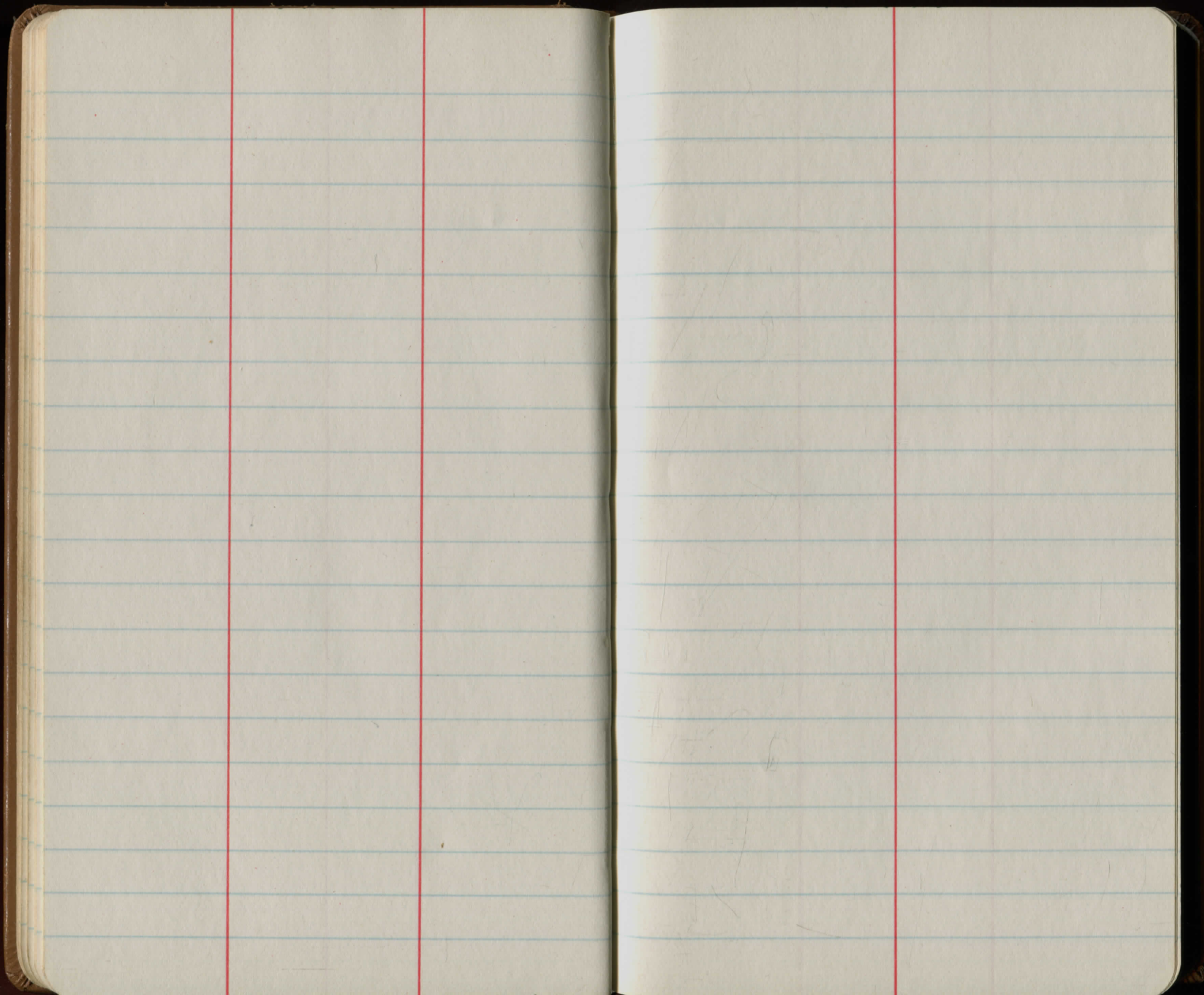


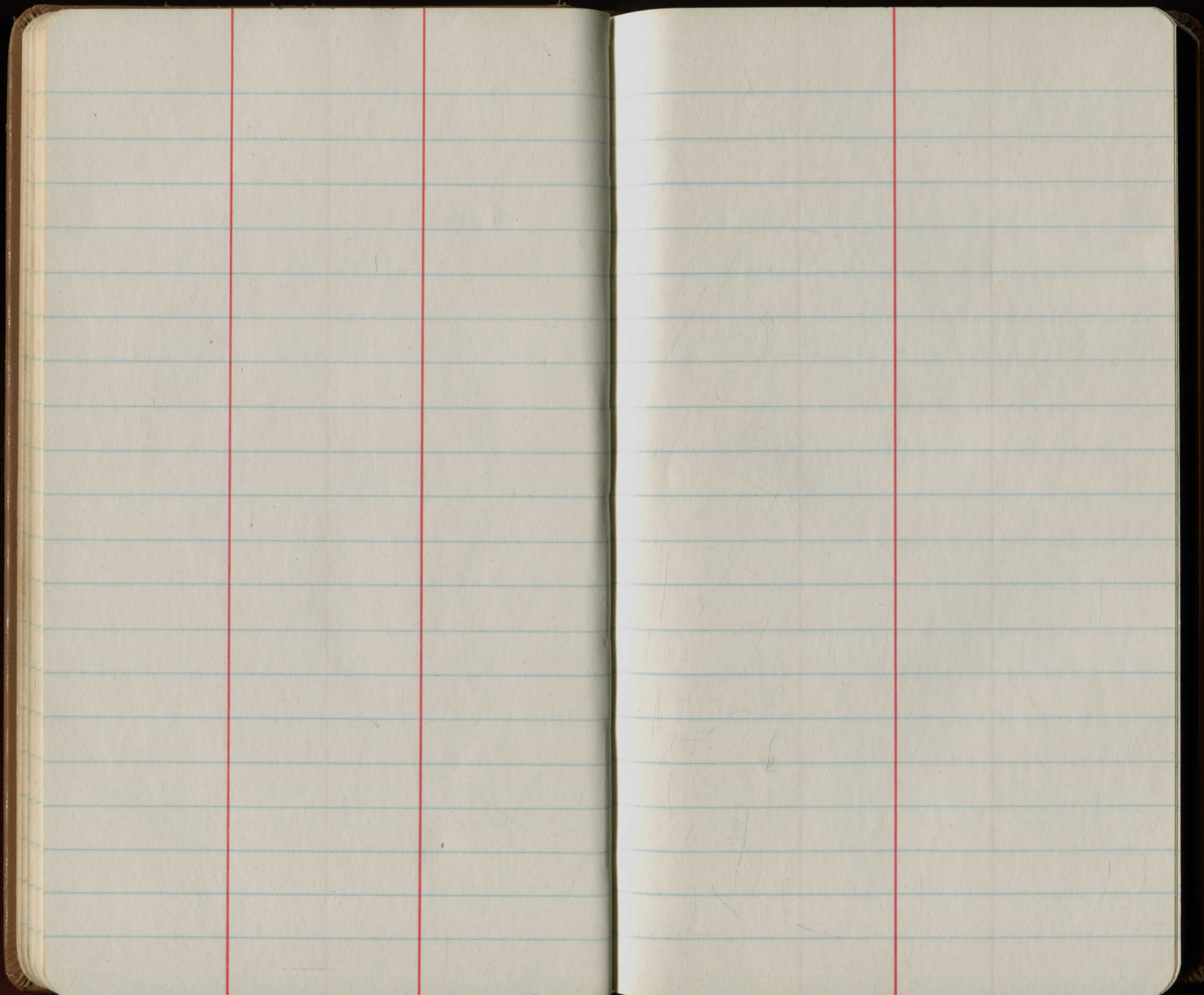


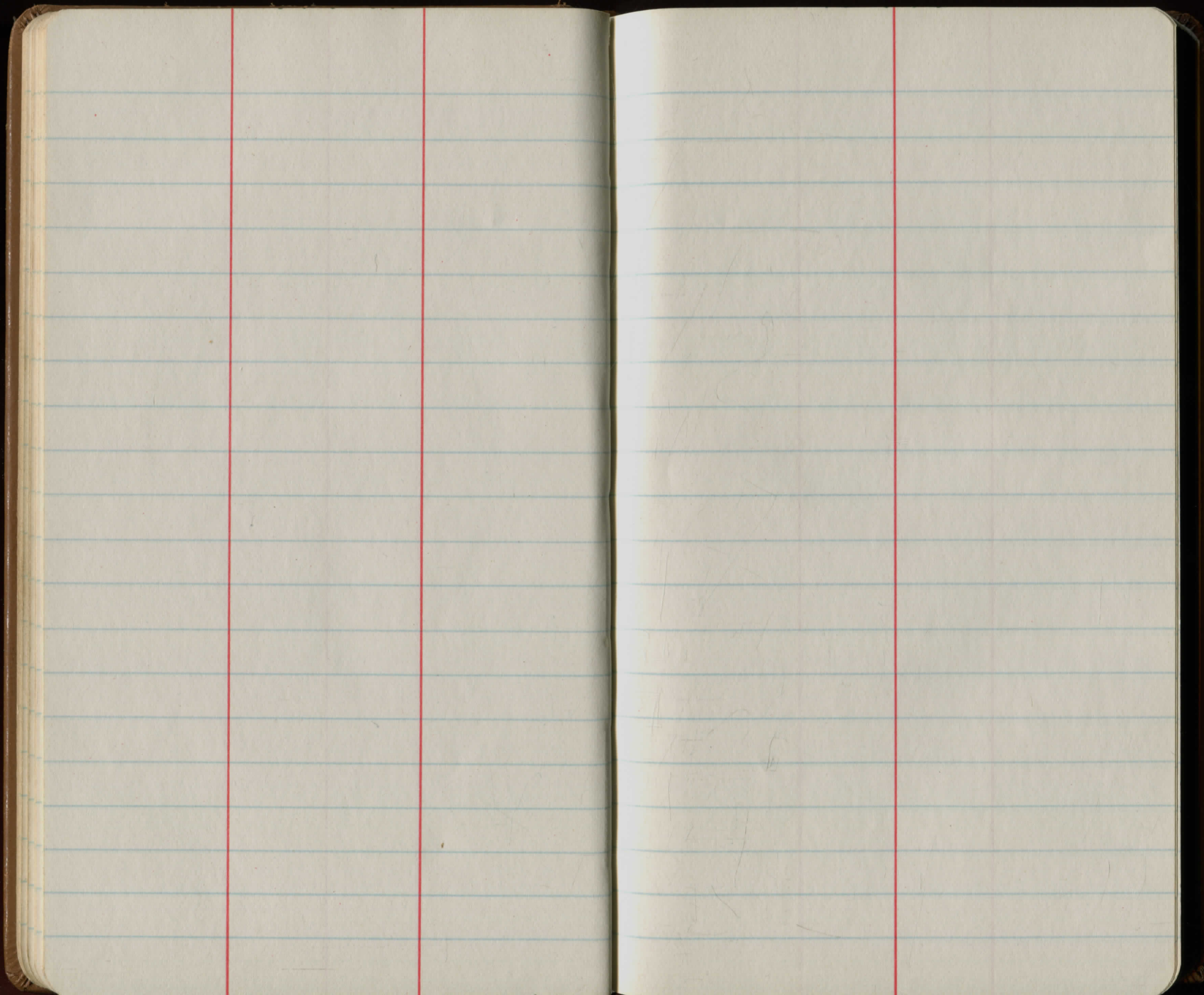


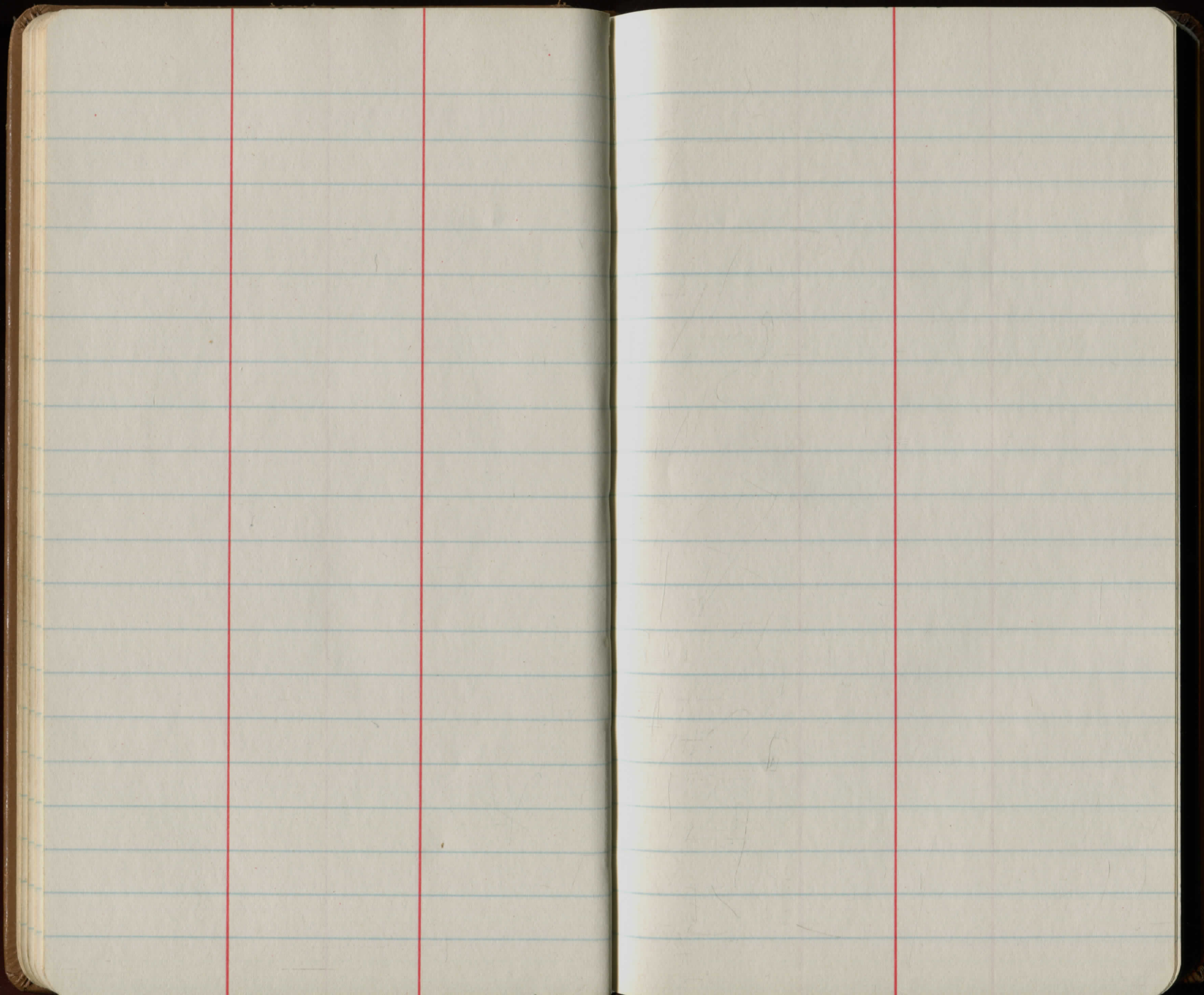


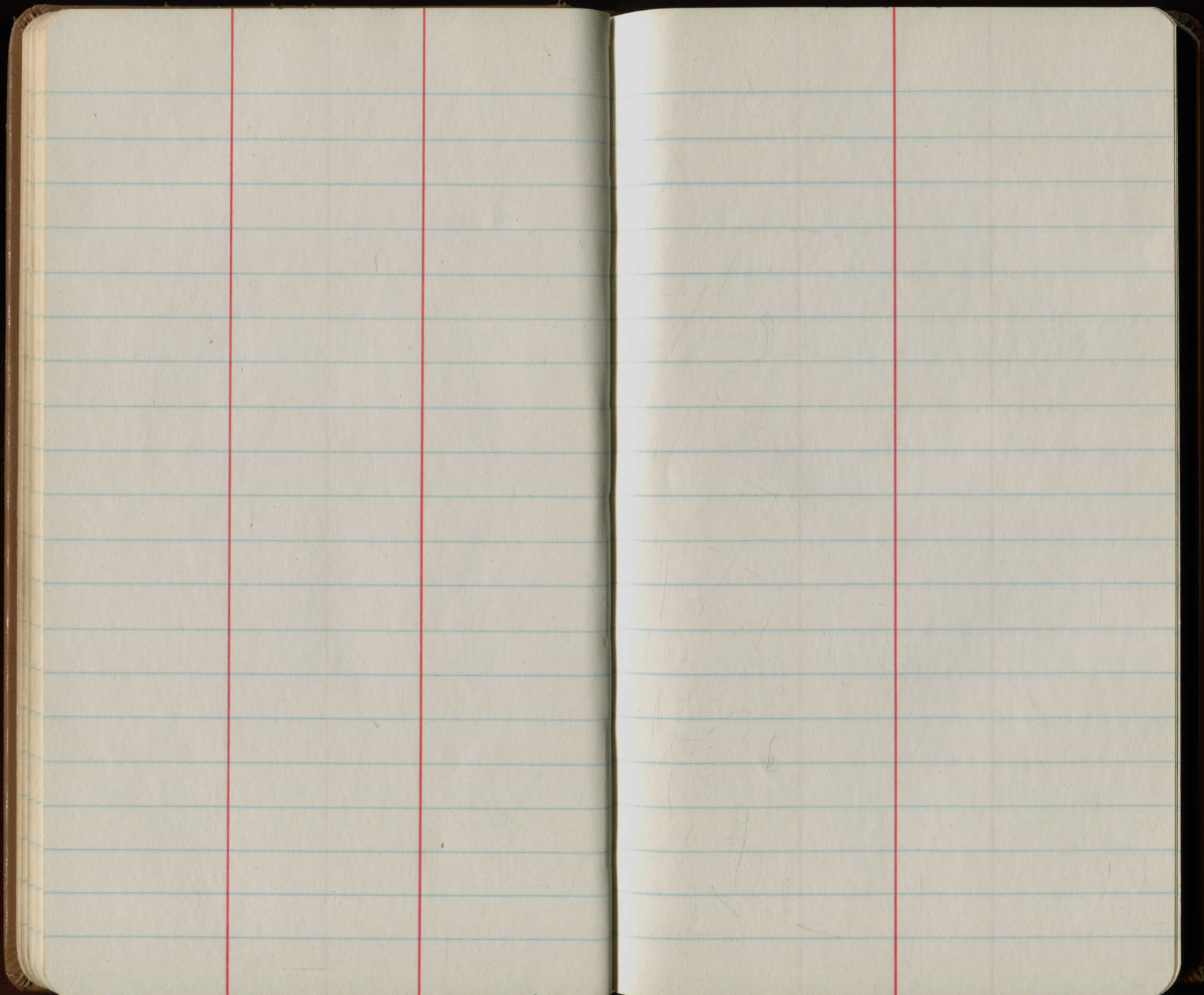












**TABLE I**

Deflections for Sub Chords for Short Radius Curves.

Degree of Curve	Radius 50 sin. def. ang.	$\frac{1/2 \text{ sub chord}}{R} = \sin. \text{ of def. angle}$				Length of arc for 100 ft.
		12.5 Ft.	15 Ft.	20 Ft.	25 Ft.	
30°	193.18	1° 51'	2° 17'	2° 58'	3° 43'	101.15
32°	181.39	1° 59'	2° 25'	3° 10'	3° 58'	101.33
34°	171.01	2° 06'	2° 33'	3° 21'	4° 12'	101.48
36°	161.80	2° 13'	2° 41'	3° 33'	4° 26'	101.66
38°	153.58	2° 20'	2° 49'	3° 44'	4° 40'	101.85
40°	146.19	2° 27'	2° 57'	3° 55'	4° 54'	102.06
42°	139.52	2° 34'	3° 05'	4° 07'	5° 08'	102.29
44°	133.47	2° 41'	3° 13'	4° 18'	5° 22'	102.53
46°	127.97	2° 48'	3° 21'	4° 29'	5° 36'	102.76
48°	122.92	2° 55'	3° 29'	4° 40'	5° 50'	103.00
50°	118.31	3° 02'	3° 38'	4° 51'	6° 04'	103.24
52°	114.06	3° 09'	3° 46'	5° 02'	6° 17'	103.54
54°	110.11	3° 16'	3° 54'	5° 13'	6° 31'	103.84
56°	106.50	3° 22'	4° 02'	5° 23'	6° 44'	104.14
58°	103.14	3° 29'	4° 10'	5° 34'	6° 57'	104.43
60°	100.00	3° 35'	4° 18'	5° 44'	7° 11'	104.72

**CURVE FORMULAS**

$T = R \tan \frac{1}{2} I$ $T = \frac{50 \tan \frac{1}{2} I}{\sin D}$ $\sin D = \frac{50}{R}$ $\sin D = \frac{50 \tan \frac{1}{2} I}{T}$	$R = T \cot \frac{1}{2} I$ $R = \frac{50}{\sin D}$ $E = R \operatorname{exsec} \frac{1}{2} I$ $E = T \tan \frac{1}{4} I$	$\text{Chord def} = \frac{\text{chord}^2}{R}$ $\text{No. chords} = \frac{1/2 I}{D}$ $\text{Tan. def.} = 1/2 \text{ chord def.}$
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The square of any distance, divided by twice the radius, will equal the distance from tangent to curve, very nearly.

Table II. contains Tangents and Externals to a 1° curve. Tan. and Ext. to any other radius may be found, nearly enough, by dividing the Tan. or Ext. opposite the given Central Angle by the given degree of curve.

To find Deg. of Curve, having the Central Angle and Tangent: Divide Tan. opposite the given Central Angle by the given Tangent.

To find Deg. of Curve, having the Central Angle and External: Divide Ext. opposite the given Central Angle by the given External.

To find Natural Tangent and Natural Exsecant for any angle by Table II.: Tan. or Ext. of twice the given angle divided by the radius of a 1° curve will be the Natural Tangent or Natural Exsecant.

To find angle for a given distance and deflection.

Rule 1. Multiply the given distance by .01745 (def. for 1° for 1 ft.), and divide given deflection by the product.

Rule 2. Multiply given deflection by 57.3, and divide the product by the given distance.

To find deflection for a given angle and distance: Multiply the angle by .01745, and the product by the distance.

**RIGHT ANGLE TRIANGLES.**—Square the altitude, divide by twice the base. Add quotient to base for hypotenuse.

Given Base 100, Alt. 10.  $10^2 \div 200 = .5$ .  $100 + .5 = 100.5$  hyp.

Given Hyp. 100, Alt. 25.  $25^2 \div 200 = 3.125$ .  $100 - 3.125 = 96.875 =$  Base  
Error in first example, .002; in last, .045.

To find Tons of Rail in one mile of track: multiply weight per yard by 11, and divide by 7.

TABLE II. Tangents and Externals to a 1° Curve

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
1°	50.00	.218	11°	551.70	26.500	21°	1061.9	97.577
10°	58.34	.297	10°	560.11	27.313	10°	1070.6	99.155
20°	66.67	.388	20°	568.53	28.137	20°	1079.2	100.75
30°	75.01	.491	30°	576.95	28.974	30°	1087.8	102.35
40°	83.34	.606	40°	585.36	29.824	40°	1096.4	103.97
50°	91.68	.733	50°	593.79	30.686	50°	1105.1	105.60
2°	100.01	.873	12°	602.21	31.561	22°	1113.7	107.24
10°	108.35	1.024	10°	610.64	32.447	10°	1122.4	108.90
20°	116.68	1.188	20°	619.07	33.347	20°	1131.0	110.57
30°	125.02	1.364	30°	627.50	34.259	30°	1139.7	112.25
40°	133.36	1.552	40°	635.93	35.183	40°	1148.4	113.95
50°	141.70	1.752	50°	644.37	36.120	50°	1157.0	115.66
3°	150.04	1.964	13°	652.81	37.070	23°	1165.7	117.38
10°	158.38	2.188	10°	661.25	38.031	10°	1174.4	119.12
20°	166.72	2.425	20°	669.70	39.006	20°	1183.1	120.87
30°	175.06	2.674	30°	678.15	39.993	30°	1191.8	122.63
40°	183.40	2.934	40°	686.60	40.992	40°	1200.5	124.41
50°	191.74	3.207	50°	695.06	42.004	50°	1209.2	126.20
4°	200.08	3.492	14°	703.51	43.029	24°	1217.9	128.00
10°	208.43	3.790	10°	711.97	44.066	10°	1226.6	129.82
20°	216.77	4.099	20°	720.44	45.116	20°	1235.3	131.65
30°	225.12	4.421	30°	728.90	46.178	30°	1244.0	133.50
40°	233.47	4.755	40°	737.37	47.253	40°	1252.8	135.35
50°	241.81	5.100	50°	745.85	48.341	50°	1261.5	137.23
5°	250.16	5.459	15°	754.32	49.441	25°	1270.2	139.11
10°	258.51	5.829	10°	762.80	50.554	10°	1279.0	141.01
20°	266.86	6.211	20°	771.29	51.679	20°	1287.7	142.93
30°	275.21	6.606	30°	779.77	52.818	30°	1296.5	144.85
40°	283.57	7.013	40°	788.26	53.969	40°	1305.3	146.79
50°	291.92	7.432	50°	796.75	55.132	50°	1314.0	148.75
6°	300.28	7.863	16°	805.25	56.309	26°	1322.8	150.71
10°	308.64	8.307	10°	813.75	57.498	10°	1331.6	152.69
20°	316.99	8.762	20°	822.25	58.699	20°	1340.4	154.69
30°	325.35	9.230	30°	830.76	59.914	30°	1349.2	156.70
40°	333.71	9.710	40°	839.27	61.141	40°	1358.0	158.72
50°	342.08	10.202	50°	847.78	62.381	50°	1366.8	160.76
7°	350.44	10.707	17°	856.30	63.634	27°	1375.6	162.81
10°	358.81	11.224	10°	864.82	64.900	10°	1384.4	164.86
20°	367.17	11.753	20°	873.35	66.178	20°	1393.2	166.95
30°	375.54	12.294	30°	881.88	67.470	30°	1402.0	169.04
40°	383.91	12.847	40°	890.41	68.774	40°	1410.9	171.15
50°	392.28	13.413	50°	898.95	70.091	50°	1419.7	173.27
8°	400.66	13.991	18°	907.49	71.421	28°	1428.6	175.41
10°	409.03	14.582	10°	916.03	72.764	10°	1437.4	177.55
20°	417.41	15.184	20°	924.58	74.119	20°	1446.3	179.72
30°	425.79	15.799	30°	933.13	75.488	30°	1455.1	181.89
40°	434.17	16.426	40°	941.69	76.869	40°	1464.0	184.08
50°	442.55	17.065	50°	950.25	78.264	50°	1472.9	186.29
9°	450.93	17.717	19°	958.81	79.671	29°	1481.8	188.51
10°	459.32	18.381	10°	967.38	81.092	10°	1490.7	190.74
20°	467.71	19.058	20°	975.96	82.525	20°	1499.6	192.99
30°	476.10	19.746	30°	984.53	83.972	30°	1508.5	195.25
40°	484.49	20.447	40°	993.12	85.431	40°	1517.4	197.53
50°	492.88	21.161	50°	1001.7	86.904	50°	1526.3	199.82
10°	501.28	21.887	20°	1010.3	88.389	30°	1535.3	202.12
10°	509.68	22.624	10°	1018.9	89.888	10°	1544.2	204.44
20°	518.08	23.375	20°	1027.5	91.399	20°	1553.1	206.77
30°	526.48	24.138	30°	1036.1	92.924	30°	1562.1	209.12
40°	534.89	24.913	40°	1044.7	94.462	40°	1571.0	211.48
50°	543.29	25.700	50°	1053.3	96.013	50°	1580.0	213.86

$T = R \tan \frac{1}{2} I$

$E = R \operatorname{exsec} \frac{1}{2} I$

TABLE II. Tangents and Externals to a 1° Curve

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
31°	1589.0	216.3	41°	2142.2	387.4	51°	2732.9	618.4
10°	1598.0	218.7	10°	2151.7	390.7	10°	2743.1	622.8
20°	1606.9	221.1	20°	2161.2	394.1	20°	2753.4	627.2
30°	1615.9	223.5	30°	2170.8	397.4	30°	2763.7	631.7
40°	1624.9	226.0	40°	2180.3	400.8	40°	2773.9	636.2
50°	1633.9	228.4	50°	2189.9	404.2	50°	2784.2	640.7
32°	1643.0	230.9	42°	2199.4	407.6	52°	2794.5	645.2
10°	1652.0	233.4	10°	2209.0	411.1	10°	2804.9	649.7
20°	1661.0	235.9	20°	2218.6	414.5	20°	2815.2	654.3
30°	1670.0	238.4	30°	2228.1	418.0	30°	2825.6	658.8
40°	1679.1	241.0	40°	2237.7	421.4	40°	2835.9	663.4
50°	1688.1	243.5	50°	2247.3	425.0	50°	2846.3	668.0
33°	1697.2	246.1	43°	2257.0	428.5	53°	2856.7	672.7
10°	1706.3	248.7	10°	2266.6	432.0	10°	2867.1	677.3
20°	1715.3	251.3	20°	2276.2	435.6	20°	2877.5	682.0
30°	1724.4	253.9	30°	2285.9	439.2	30°	2888.0	686.7
40°	1733.5	256.5	40°	2295.6	442.8	40°	2898.4	691.4
50°	1742.6	259.1	50°	2305.2	446.4	50°	2908.9	696.1
34°	1751.7	261.8	44°	2314.9	450.0	54°	2919.4	700.9
10°	1760.8	264.5	10°	2324.6	453.6	10°	2929.9	705.7
20°	1770.0	267.2	20°	2334.3	457.3	20°	2940.4	710.5
30°	1779.1	269.9	30°	2344.1	461.0	30°	2951.0	715.3
40°	1788.2	272.6	40°	2353.8	464.6	40°	2961.5	720.1
50°	1797.4	275.3	50°	2363.5	468.4	50°	2972.1	725.0
35°	1806.6	278.1	45°	2373.3	472.1	55°	2982.7	729.9
10°	1815.7	280.8	10°	2383.1	475.8	10°	2993.3	734.8
20°	1824.9	283.6	20°	2392.8	479.6	20°	3003.9	739.7
30°	1834.1	286.4	30°	2402.6	483.4	30°	3014.5	744.6
40°	1843.3	289.2	40°	2412.4	487.2	40°	3025.2	749.6
50°	1852.5	292.0	50°	2422.3	491.0	50°	3035.8	754.6
36°	1861.7	294.9	46°	2432.1	494.8	56°	3046.5	759.6
10°	1870.9	297.7	10°	2441.9	498.7	10°	3057.2	764.6
20°	1880.1	300.6	20°	2451.8	502.5	20°	3067.9	769.7
30°	1889.4	303.5	30°	2461.7	506.4	30°	3078.7	774.7
40°	1898.6	306.4	40°	2471.5	510.3	40°	3089.4	779.8
50°	1907.9	309.3	50°	2481.4	514.3	50°	3100.2	784.9
37°	1917.1	312.2	47°	2491.3	518.2	57°	3110.9	790.1
10°	1926.4	315.2	10°	2501.2	522.2	10°	3121.7	795.2
20°	1935.7	318.1	20°	2511.2	526.1	20°	3132.6	800.4
30°	1945.0	321.1	30°	2521.1	530.1	30°	3143.4	805.6
40°	1954.3	324.1	40°	2531.1	534.2	40°	3154.2	810.9
50°	1963.6	327.1	50°	2541.0	538.2	50°	3165.1	816.1
38°	1972.9	330.2	48°	2551.0	542.2	58°	3176.0	821.4
10°	1982.2	333.2	10°	2561.0	546.3	10°	3186.9	826.7
20°	1991.5	336.3	20°	2571.0	550.4	20°	3197.8	832.0
30°	2000.9	339.3	30°	2581.0	554.5	30°	3208.8	837.3
40°	2010.2	342.4	40°	2591.0	558.6	40°	3219.7	842.7
50°	2019.6	345.5	50°	2601.1	562.8	50°	3230.7	848.1
39°	2029.0	348.6	49°	2611.2	566.9	59°	3241.7	853.5
10°	2038.4	351.8	10°	2621.2	571.1	10°	3252.7	858.9
20°	2047.8	354.9	20°	2631.3	575.3	20°	3263.7	864.3
30°	2057.2	358.1	30°	2641.4	579.5	30°	3274.8	869.8
40°	2066.6	361.3	40°	2651.5	583.8	40°	3285.8	875.3
50°	2076.0	364.5	50°	2661.6	588.0	50°	3296.9	880.8
40°	2085.4	367.7	50°	2671.8	592.3	60°	3308.0	886.4
10°	2094.9	371.0	10°	2681.9	596.6	10°	3319.1	892.0
20°	2104.3	374.2	20°	2692.1	600.9	20°	3330.3	897.5
30°	2113.8	377.5	30°	2702.3	605.3	30°	3341.4	903.2
40°	2123.3	380.8	40°	2712.5	609.6	40°	3352.6	908.8
50°	2132.7	384.1	50°	2722.7	614.0	50°	3363.8	914.5

$T = R \tan \frac{1}{2} I$

$E = R \operatorname{exsec} \frac{1}{2} I$

TABLE II. Tangents and Externals to a 1° Curve

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
61°	3375.0	920.2	71°	4086.9	1308.2	81°	4893.6	1805.3
10'	3386.3	925.9	10'	4099.5	1315.6	10'	4908.0	1814.7
20'	3397.5	931.6	20'	4112.1	1322.9	20'	4922.5	1824.1
30'	3408.8	937.3	30'	4124.8	1330.3	30'	4937.0	1833.6
40'	3420.1	943.1	40'	4137.4	1337.7	40'	4951.5	1843.1
50'	3431.4	948.9	50'	4150.1	1345.1	50'	4966.1	1852.6
62°	3442.7	954.8	72°	4162.8	1352.6	82°	4980.7	1862.2
10'	3454.1	960.6	10'	4175.6	1360.1	10'	4995.4	1871.8
20'	3465.4	966.5	20'	4188.5	1367.6	20'	5010.0	1881.5
30'	3476.8	972.4	30'	4201.2	1375.2	30'	5024.8	1891.2
40'	3488.3	978.3	40'	4214.0	1382.8	40'	5039.5	1900.9
50'	3499.7	984.3	50'	4226.8	1390.4	50'	5054.3	1910.7
63°	3511.1	990.2	73°	4239.7	1398.0	83°	5069.2	1920.5
10'	3522.6	996.2	10'	4252.6	1405.7	10'	5084.0	1930.2
20'	3534.1	1002.3	20'	4265.6	1413.5	20'	5099.0	1940.3
30'	3545.6	1008.3	30'	4278.5	1421.2	30'	5113.9	1950.3
40'	3557.2	1014.4	40'	4291.5	1429.0	40'	5128.9	1960.2
50'	3568.7	1020.5	50'	4304.6	1436.8	50'	5143.9	1970.3
64°	3580.3	1026.6	74°	4317.6	1444.6	84°	5159.0	1980.4
10'	3591.9	1032.8	10'	4330.7	1452.5	10'	5174.1	1990.5
20'	3603.5	1039.0	20'	4343.8	1460.4	20'	5189.3	2000.6
30'	3615.1	1045.2	30'	4356.9	1468.4	30'	5204.4	2010.8
40'	3626.8	1051.4	40'	4370.1	1476.4	40'	5219.7	2021.1
50'	3638.5	1057.7	50'	4383.3	1484.4	50'	5234.9	2031.4
65°	3650.2	1063.9	75°	4396.5	1492.4	85°	5250.3	2041.7
10'	3661.9	1070.2	10'	4409.8	1500.5	10'	5265.6	2052.1
20'	3673.7	1076.6	20'	4423.1	1508.6	20'	5281.0	2062.5
30'	3685.4	1082.9	30'	4436.4	1516.7	30'	5296.4	2073.0
40'	3697.2	1089.3	40'	4449.7	1524.9	40'	5311.9	2083.5
50'	3709.0	1095.7	50'	4463.1	1533.1	50'	5327.4	2094.1
66°	3720.9	1102.2	76°	4476.5	1541.4	86°	5343.0	2104.7
10'	3732.7	1108.6	10'	4489.9	1549.7	10'	5358.6	2115.3
20'	3744.6	1115.1	20'	4503.4	1558.0	20'	5374.2	2126.0
30'	3756.5	1121.7	30'	4516.9	1566.3	30'	5389.9	2136.7
40'	3768.5	1128.2	40'	4530.4	1574.7	40'	5405.6	2147.5
50'	3780.4	1134.8	50'	4544.0	1583.1	50'	5421.4	2158.4
67°	3792.4	1141.4	77°	4557.6	1591.6	87°	5437.2	2169.2
10'	3804.4	1148.0	10'	4571.2	1600.1	10'	5453.1	2180.2
20'	3816.4	1154.7	20'	4584.8	1608.6	20'	5469.0	2191.1
30'	3828.4	1161.3	30'	4598.5	1617.1	30'	5484.9	2202.2
40'	3840.5	1168.1	40'	4612.2	1625.7	40'	5500.9	2213.2
50'	3852.6	1174.8	50'	4626.0	1634.4	50'	5517.0	2224.3
68°	3864.7	1181.6	78°	4639.8	1643.0	88°	5533.1	2235.5
10'	3876.8	1188.4	10'	4653.6	1651.7	10'	5549.2	2246.7
20'	3889.0	1195.2	20'	4667.4	1660.5	20'	5565.4	2258.0
30'	3901.2	1202.0	30'	4681.3	1669.2	30'	5581.6	2269.3
40'	3913.4	1208.9	40'	4695.2	1678.1	40'	5597.8	2280.6
50'	3925.6	1215.8	50'	4709.2	1686.9	50'	5614.2	2292.0
69°	3937.9	1222.7	79°	4723.2	1695.8	89°	5630.5	2303.5
10'	3950.2	1229.7	10'	4737.2	1704.7	10'	5646.9	2315.0
20'	3962.5	1236.7	20'	4751.2	1713.7	20'	5663.4	2326.6
30'	3974.8	1243.7	30'	4765.3	1722.7	30'	5679.9	2338.2
40'	3987.2	1250.8	40'	4779.4	1731.7	40'	5696.4	2349.8
50'	3999.5	1257.9	50'	4793.6	1740.8	50'	5713.0	2361.5
70°	4011.9	1265.0	80°	4807.7	1749.9	90°	5729.7	2373.5
10'	4024.4	1272.1	10'	4822.0	1759.0	10'	5746.3	2385.1
20'	4036.8	1279.3	20'	4836.2	1768.2	20'	5763.1	2397.0
30'	4049.3	1286.5	30'	4850.5	1777.4	30'	5779.9	2408.9
40'	4061.8	1293.6	40'	4864.8	1786.6	40'	5796.7	2420.9
50'	4074.4	1300.9	50'	4879.2	1796.0	50'	5813.6	2432.9

$$T = R \tan \frac{1}{2} I$$

$$E = R \operatorname{exsec} \frac{1}{2} I$$

TABLE II. Tangents and Externals to a 1° Curve

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
91°	5830.5	2444.9	101°	6950.6	3278.1	111°	8336.7	4386.1
10'	5847.5	2457.1	10'	6971.3	3294.1	10'	8362.7	4407.6
20'	5864.6	2469.3	20'	6992.0	3310.1	20'	8388.9	4429.2
30'	5881.7	2481.5	30'	7012.7	3326.1	30'	8415.1	4450.9
40'	5898.8	2493.8	40'	7033.6	3342.3	40'	8441.5	4472.7
50'	5916.0	2506.1	50'	7054.5	3358.5	50'	8468.0	4494.6
92°	5932.2	2518.5	102°	7075.5	3374.9	112°	8494.6	4516.6
10'	5950.5	2531.0	10'	7096.6	3391.2	10'	8521.3	4538.8
20'	5967.9	2543.5	20'	7117.8	3407.7	20'	8548.1	4561.1
30'	5985.3	2556.0	30'	7139.0	3424.3	30'	8575.0	4583.4
40'	6002.7	2568.6	40'	7160.3	3440.9	40'	8602.1	4606.0
50'	6020.2	2581.3	50'	7181.7	3457.6	50'	8629.3	4628.6
93°	6037.8	2594.0	103°	7203.2	3474.4	113°	8656.6	4651.3
10'	6055.4	2606.8	10'	7224.7	3491.3	10'	8684.0	4674.2
20'	6073.1	2619.7	20'	7246.3	3508.2	20'	8711.5	4697.2
30'	6090.8	2632.6	30'	7268.0	3525.2	30'	8739.2	4720.3
40'	6108.6	2645.4	40'	7289.8	3542.4	40'	8767.0	4743.6
50'	6126.4	2658.5	50'	7311.7	3559.6	50'	8794.9	4766.9
94°	6144.3	2671.6	104°	7333.6	3576.8	114°	8822.9	4790.4
10'	6162.2	2684.7	10'	7355.6	3594.2	10'	8851.0	4814.1
20'	6180.2	2697.9	20'	7377.8	3611.7	20'	8879.3	4837.8
30'	6198.3	2711.2	30'	7399.9	3629.2	30'	8907.7	4861.7
40'	6216.4	2724.5	40'	7422.2	3646.8	40'	8936.3	4885.7
50'	6234.6	2737.9	50'	7444.6	3664.5	50'	8965.0	4909.9
95°	6252.8	2751.3	105°	7467.0	3682.3	115°	8993.8	4934.1
10'	6271.1	2764.8	10'	7489.6	3700.2	10'	9022.7	4958.6
20'	6289.4	2778.3	20'	7512.2	3718.2	20'	9051.7	4983.1
30'	6307.9	2792.0	30'	7534.9	3736.2	30'	9080.9	5007.8
40'	6326.3	2805.6	40'	7557.7	3754.4	40'	9110.3	5032.6
50'	6344.8	2819.4	50'	7580.5	3772.6	50'	9139.8	5057.6
96°	6363.4	2833.2	106°	7603.5	3791.0	116°	9169.4	5082.7
10'	6382.1	2847.0	10'	7626.6	3809.4	10'	9199.1	5107.9
20'	6400.8	2861.0	20'	7649.7	3827.9	20'	9229.0	5133.3
30'	6419.5	2875.0	30'	7672.9	3846.5	30'	9259.0	5158.8
40'	6438.4	2889.0	40'	7696.3	3865.2	40'	9289.2	5184.5
50'	6457.3	2903.1	50'	7719.7	3884.0	50'	9319.5	5210.3
97°	6476.2	2917.3	107°	7743.2	3902.9	117°	9349.9	5236.2
10'	6495.2	2931.6	10'	7766.8	3921.9	10'	9380.5	5262.3
20'	6514.3	2945.9	20'	7790.5	3940.9	20'	9411.3	5288.6
30'	6533.4	2960.3	30'	7814.3	3960.1	30'	9442.2	5315.0
40'	6552.6	2974.7	40'	7838.1	3979.4	40'	9473.2	5341.5
50'	6571.9	2989.2	50'	7862.1	3998.7	50'	9504.4	5368.2
98°	6591.2	3003.8	108°	7886.2	4018.2	118°	9535.7	5395.1
10'	6610.6	3018.4	10'	7910.4	4037.8	10'	9567.2	5422.1
20'	6630.1	3033.1	20'	7934.6	4057.4	20'	9598.9	5449.2
30'	6649.6	3047.9	30'	7959.0	4077.2	30'	9630.7	5476.5
40'	6669.2	3062.8	40'	7983.5	4097.1	40'	9662.6	5504.0
50'	6688.8	3077.7	50'	8008.0	4117.0	50'	9694.7	5531.7
99°	6708.6	3092.7	109°	8032.7	4137.1	119°	9727.0	5559.4
10'	6728.4	3107.7	10'	8057.4	4157.3	10'	9759.4	5587.4
20'	6748.2	3122.9	20'	8082.3	4177.5	20'	9792.0	5615.5
30'	6768.1	3138.1	30'	8107.3	4197.9	30'	9824.8	5643.8
40'	6788.1	3153.3	40'	8132.3	4218.4	40'	9857.7	5672.3
50'	6808.2	3168.7	50'	8157.5	4239.0	50'	9890.8	5700.9
100°	6828.3	3184.1	110°	8182.8	4259.7	120°	9924.0	5729.7
10'	6848.5	3199.6	10'	8208.2	4280.5	10'	9957.5	5758.6
20'	6868.8	3215.1	20'	8233.7	4301.2	20'	9991.0	5787.7
30'	6889.2	3230.8	30'	8259.3	4322.4	30'	10025.0	5817.0
40'	6909.6	3246.5	40'	8285.0	4343.6	40'	10059.0	5846.5
50'	6930.1	3262.3	50'	8310.8	4364.8	50'	10093.0	5876.1

$$T = R \tan \frac{1}{2} I$$

$$E = R \operatorname{exsec} \frac{1}{2} I$$

**TABLE III. CORRECTIONS FOR USE WITH TABLE II**

For Tangents Add  
Degree of Curve

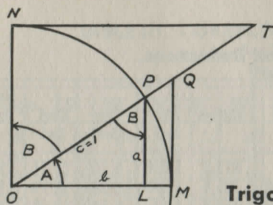
Angle	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.49	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34

For Externals Add  
Degree of Curve

Angle	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96

**TABLE IV**  
Radii, Ordinates and Deflections.

Deg.	Radius	Mid. Ord.	Tan. Def.	Chd. Def.	Def. for 1 Foot	Deg.	Radius	Mid. Ord.	Tan. Def.	Chd. Def.	Def. for 1 Foot
0° 10'	34377.	.036	.145	.291	0.05'	7°	819.0	1.528	6.105	12.21	2.10'
20	17189.	.073	.291	.582	0.10	20'	781.8	1.600	6.395	12.79	2.20
30	11459.	.109	.436	.873	0.15	30	764.5	1.637	6.540	13.08	2.25
40	8594.4	.145	.582	1.164	0.20	40	747.9	1.673	6.685	13.37	2.30
50	6875.5	.182	.727	1.454	0.25	8	716.8	1.746	6.976	13.95	2.40
1	5729.6	.218	.873	1.745	0.30	20	688.2	1.819	7.266	14.53	2.50
10	4911.2	.255	1.018	2.036	0.35	30	674.7	1.855	7.411	14.82	2.55
20	4297.3	.291	1.164	2.327	0.40	40	661.7	1.892	7.556	15.11	2.60
30	3819.8	.327	1.309	2.618	0.45	9	637.3	1.965	7.846	15.69	2.70
40	3437.9	.364	1.454	2.909	0.50	20	614.6	2.037	8.136	16.27	2.80
50	3125.4	.400	1.600	3.200	0.55	30	603.8	2.074	8.281	16.56	2.85
2	2864.9	.436	1.745	3.490	0.60	40	593.4	2.110	8.426	16.85	2.90
10	2644.6	.473	1.891	3.781	0.65	10	573.7	2.183	8.716	17.43	3.00
20	2455.7	.509	2.036	4.072	0.70	30	546.4	2.292	9.150	18.30	3.15
30	2290.0	.545	2.181	4.363	0.75	11	521.7	2.402	9.585	19.16	3.30
40	2148.8	.582	2.327	4.654	0.80	30	499.1	2.511	10.02	20.04	3.45
50	2022.4	.618	2.472	4.945	0.85	12	478.3	2.620	10.45	20.91	3.60
3	1910.1	.655	2.618	5.235	0.90	30	459.3	2.730	10.89	21.77	3.75
10	1809.6	.691	2.763	5.526	0.95	13	441.7	2.839	11.32	22.64	3.90
20	1719.1	.727	2.908	5.817	1.00	30	425.4	2.949	11.75	23.51	4.05
30	1637.3	.764	3.054	6.108	1.05	14	410.3	3.058	12.18	24.37	4.20
40	1562.9	.800	3.199	6.398	1.10	30	396.2	3.168	12.62	25.24	4.35
50	1495.0	.836	3.345	6.689	1.15	15	383.1	3.277	13.05	26.11	4.50
4	1432.7	.873	3.490	6.980	1.20	30	370.8	3.387	13.49	26.97	4.65
10	1375.4	.909	3.635	7.271	1.25	16	359.3	3.496	13.92	27.84	4.80
20	1322.5	.945	3.781	7.561	1.30	30	348.5	3.606	14.35	28.70	4.95
30	1273.6	.982	3.926	7.852	1.35	17	338.3	3.716	14.78	29.56	5.10
40	1228.1	1.018	4.071	8.143	1.40	18	319.6	3.935	15.64	31.29	5.40
50	1185.8	1.055	4.217	8.433	1.45	19	302.9	4.155	16.51	33.01	5.70
5	1146.3	1.091	4.362	8.724	1.50	20	287.9	4.374	17.37	34.73	6.00
10	1109.3	1.127	4.507	9.014	1.55	21	274.4	4.594	18.22	36.44	6.30
20	1074.7	1.164	4.653	9.305	1.60	22	262.0	4.814	19.08	38.16	6.60
30	1042.1	1.200	4.798	9.596	1.65	23	250.8	5.035	19.94	39.87	6.90
40	1011.5	1.237	4.943	9.886	1.70	24	240.5	5.255	20.79	41.58	7.20
50	982.6	1.273	5.088	10.18	1.75	25	231.0	5.476	21.64	43.28	7.50
6	955.4	1.309	5.234	10.47	1.80	26	222.3	5.697	22.50	44.99	7.80
10	929.6	1.346	5.379	10.76	1.85	27	214.2	5.918	23.35	46.69	8.10
20	905.1	1.382	5.524	11.05	1.90	28	206.7	6.139	24.19	48.38	8.40
30	881.9	1.418	5.669	11.34	1.95	29	199.7	6.360	25.04	50.07	8.70
40	859.9	1.455	5.814	11.63	2.00	30	193.2	6.583	25.88	51.76	9.00



**TABLE V**

**Trigonometric Formulae**

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OP = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

Law of Sines  $\frac{\sin A}{a} = \frac{\sin B}{b} = \frac{\sin C}{c}$

Law of Cosines  $c^2 = a^2 + b^2 - 2ab \cos C$

Law of Tangents  $\frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$

In any triangle:

Given  $a, b, C$ ; to find  $c, B, A$ .

Use Law of Sines.

Given  $A, B, c$ ; to find  $a, b, C$ .

Use Law of Sines.

Given  $a, b, c$ ; to find  $A, B, C$ .

$$\text{Let } \frac{a+b+c}{2} = s: \quad \sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = r$$

**Trigonometric Formulae (continued)**

$$\cos \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}} \quad \tan \frac{1}{2} B = \frac{r}{s-b}$$

$$\tan \frac{1}{2} A = \frac{r}{s-a} \quad \tan \frac{1}{2} C = \frac{r}{s-c}$$

$$\text{Area of a triangle: Area} = \frac{1}{2} ab \sin C = \sqrt{s(s-a)(s-b)(s-c)}$$

**Prismoidal Formula**

$$\text{Vol.} = \frac{h}{6} (B+b+4M)$$

$h$  = altitude;  $b, B$  = bases;  $M$  = midsection

**TABLE VI**

**Minutes in Decimals of a Degree.**

0' 30"	.00833	10' 30"	.17500	20' 30"	.34167	30' 30"	.50833	40' 30"	.67500	50' 30"	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000

**TABLE VII**

**Inches and Fractions of an Inch in Decimals of a Foot**

	0	1	2	3	4	5	6	7	8	9	10	11	
$\frac{1}{16}$	.0052	.0885	.1719	.2552	.3385	.4219	.5052	.5885	.6719	.7552	.8385	.9219	$\frac{1}{16}$
$\frac{1}{8}$	.0104	.0938	.1771	.2604	.3438	.4271	.5104	.5938	.6771	.7604	.8438	.9271	$\frac{1}{8}$
$\frac{3}{16}$	.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323	$\frac{3}{16}$
$\frac{1}{4}$	.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375	$\frac{1}{4}$
$\frac{5}{16}$	.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	.6927	.7760	.8594	.9427	$\frac{5}{16}$
$\frac{3}{8}$	.0313	.1146	.1979	.2813	.3646	.4479	.5313	.6146	.6979	.7813	.8646	.9479	$\frac{3}{8}$
$\frac{7}{16}$	.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531	$\frac{7}{16}$
$\frac{1}{2}$	.0417	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583	$\frac{1}{2}$
$\frac{9}{16}$	.0469	.1302	.2135	.2969	.3803	.4635	.5469	.6302	.7135	.7969	.8802	.9635	$\frac{9}{16}$
$\frac{5}{8}$	.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	.9688	$\frac{5}{8}$
$\frac{11}{16}$	.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740	$\frac{11}{16}$
$\frac{3}{4}$	.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792	$\frac{3}{4}$
$\frac{13}{16}$	.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844	$\frac{13}{16}$
$\frac{7}{8}$	.0729	.1563	.2396	.3229	.4063	.4896	.5729	.6563	.7396	.8229	.9063	.9896	$\frac{7}{8}$
$\frac{15}{16}$	.0781	.1615	.2448	.3281	.4115	.4948	.5781	.6615	.7448	.8281	.9115	.9948	$\frac{15}{16}$
1	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167	1.0000	1
	0	1	2	3	4	5	6	7	8	9	10	11	

TABLE VIII  
Sines, Cosines, Tangents, Cotangents

deg.	sin 0'	tan 0'	sin 10'	tan 10'	sin 20'	tan 20'	sin 30'	tan 30'	sin 40'	tan 40'	sin 50'	tan 50'	deg.
0	0000	0000	0029	0029	0058	0058	0087	0087	0116	0116	0145	0145	89
1	175	0175	0204	0204	0233	0233	0262	262	291	291	320	320	88
2	349	349	378	378	407	407	436	437	465	466	494	495	87
3	523	524	552	553	581	582	610	612	640	641	669	670	86
4	698	699	727	729	756	758	785	787	814	816	843	864	85
5	872	875	901	904	929	934	958	963	987	992	1016	1022	84
6	1045	1051	1074	1080	1103	1110	1132	1139	1161	1169	1190	1198	83
7	219	228	248	257	279	287	305	317	334	346	363	376	82
8	392	405	421	435	449	465	478	495	507	524	536	554	81
9	564	584	593	614	622	644	650	673	679	703	708	733	80
10	736	763	765	793	794	823	822	853	851	883	880	914	79
11	908	944	937	974	965	2004	994	2035	2022	2065	2051	2095	78
12	2079	2126	2108	2156	2136	186	2164	217	193	247	221	278	77
13	250	309	278	339	306	370	334	401	363	432	391	462	76
14	419	493	447	524	476	555	504	586	532	617	560	648	75
15	588	679	616	711	644	742	672	773	700	805	728	836	74
16	756	867	784	899	812	931	840	962	868	994	896	3026	73
17	924	3057	952	3089	2979	3121	3007	3153	3035	3185	3062	217	72
18	3090	249	3118	281	3145	314	173	346	201	378	228	411	71
19	256	443	283	476	311	508	338	541	365	574	393	607	70
20	420	640	448	673	475	706	502	739	529	772	557	805	69
21	584	839	611	872	638	906	665	939	692	973	719	4006	68
22	746	4040	773	4074	800	4108	825	4142	854	4176	881	210	67
23	907	245	934	279	961	314	987	348	4014	383	4041	417	66
24	4067	452	4094	487	4120	522	4147	557	173	592	200	628	65
25	226	663	253	699	279	734	305	770	331	806	358	841	64
26	384	877	410	913	436	950	4462	986	488	5022	514	5059	63
27	540	5095	566	5132	592	5169	617	5206	643	243	669	280	62
28	695	317	720	354	746	392	772	430	797	467	823	505	61
29	848	543	874	581	899	619	924	658	950	696	975	735	60
30	5000	774	5025	5812	5050	851	5075	890	5100	930	5125	969	59
31	150	6009	175	6048	200	6088	225	6128	250	6168	275	6208	58
32	299	249	324	289	348	330	5373	371	398	412	422	453	57
33	446	494	471	536	495	577	519	619	544	661	568	703	56
34	592	745	616	787	640	830	664	873	688	916	712	959	55
35	736	7002	760	7046	783	7089	807	7133	831	7177	854	7221	54
36	878	265	901	310	925	355	948	400	972	445	995	490	53
37	6018	536	6041	581	6065	627	6088	673	6111	720	6134	766	52
38	157	813	180	860	202	907	225	954	248	8002	271	8050	51
39	293	8098	316	8146	338	8195	361	8243	383	292	406	342	50
40	428	391	450	441	472	491	494	541	517	591	539	642	49
41	561	693	583	744	604	796	626	847	648	899	670	952	48
42	691	9004	713	9057	734	9110	756	9163	777	9217	799	9271	47
43	820	325	841	380	862	435	884	490	905	545	926	601	46
44	947	657	967	713	988	770	7009	827	7030	884	7050	942	45
45	7071	1.0000	7092	1.0058	7112	1.0117	133	1.0176	153	1.0235	173	1.0295	44
deg.	60' cos	60' cot	50' cos	50' cot	40' cos	40' cot	30' cos	30' cot	20' cos	20' cot	10' cos	10' cot	deg.

TABLE VIII (Continued)  
Sines, Cosines, Tangents, Cotangents (continued)

deg.	sin 0'	tan 0'	sin 10'	tan 10'	sin 20'	tan 20'	sin 30'	tan 30'	sin 40'	tan 40'	sin 50'	tan 50'	deg.
46	7193	1.0355	7214	1.0416	7234	1.0477	7254	1.0533	7274	1.0599	7294	1.0661	43
47	314	.0724	333	.0786	353	.0850	373	.0913	392	.0977	412	.1041	42
48	431	.1106	451	.1171	470	.1237	490	.1303	509	.1369	528	.1436	41
49	547	.1504	566	.1571	585	.1640	604	.1708	623	.1778	642	.1847	40
50	660	1.1918	7679	1.1988	7698	1.2059	7716	1.2131	7735	1.2203	7753	1.2276	39
51	771	2.349	790	2.423	808	2.497	826	2.572	844	2.647	862	2.723	38
52	880	2.799	898	2.876	916	2.954	934	3.032	951	3.111	969	3.190	37
53	986	3.270	8004	3.351	8021	3.452	8039	3.514	8056	3.597	8073	3.680	36
54	8090	3.764	107	3.848	124	3.934	141	4.019	158	4.106	175	4.193	35
55	192	4.281	208	4.370	225	4.460	241	4.550	258	4.641	274	4.733	34
56	290	4.826	307	4.919	323	5.013	339	5.108	355	5.204	371	5.301	33
57	387	5.399	403	5.497	418	5.597	434	5.697	450	5.798	465	5.900	32
58	480	6.003	496	6.107	511	6.212	526	6.319	542	6.426	557	6.534	31
59	572	6.643	587	6.753	601	6.864	616	6.977	631	7.090	646	7.205	30
60	660	1.7321	8675	1.7437	8689	1.7556	8704	1.7675	8718	1.7797	8732	1.7917	29
61	746	8.040	760	8.165	774	8.291	788	8.418	802	8.546	816	8.676	28
62	829	8.807	843	8.940	857	9.074	870	9.210	884	9.347	897	9.486	27
63	910	9.626	923	9.768	936	9.912	949	2.0057	962	2.0204	975	2.0353	26
64	988	2.0503	9001	2.0655	9013	2.0809	9026	2.0965	9038	2.1123	9051	2.1283	25
65	963	1.445	075	1.609	088	1.775	100	1.943	112	2.113	124	2.286	24
66	135	2.260	147	2.637	159	2.817	171	2.998	182	3.183	194	3.369	23
67	205	3.559	216	3.750	228	3.945	239	4.142	250	4.342	261	4.545	22
68	272	4.751	283	4.960	293	5.172	304	5.386	315	5.605	325	5.826	21
69	336	6.051	346	6.279	356	6.511	367	6.746	377	6.985	387	7.228	20
70	397	2.7475	9407	2.7725	9417	2.7980	9426	2.8239	9436	2.8502	9446	2.8770	19
71	455	9.042	465	9.319	474	9.600	483	9.887	492	3.0178	502	3.0475	18
72	511	3.0777	520	3.1084	528	3.1397	537	3.1716	546	3.2041	555	3.2371	17
73	563	2.709	572	3.052	580	3.402	588	3.759	596	4.124	605	4.495	16
74	613	4.874	621	5.261	628	5.656	636	6.059	644	6.470	652	6.891	15
75	659	7.321	667	7.760	674	8.208	681	8.657	689	9.136	696	9.617	14
76	703	4.0108	710	4.0611	717	4.1126	724	4.1653	730	4.2193	737	4.2743	13
77	744	3.315	750	3.897	757	4.494	763	5.107	769	5.736	775	6.382	12
78	781	7.046	787	7.729	793	8.430	799	9.152	805	9.894	811	5.0658	11
79	816	1.446	822	5.2257	827	5.3093	833	5.3955	838	5.4845	843	5.5764	10
80	9848	5.6713	9853	5.7694	9858	5.8708	9863	5.9758	9868	6.0844	9872	6.1970	9
81	877	6.3138	881	6.4348	886	6.5606	890	6.6912	894	6.8269	899	6.9682	8
82	903	7.1154	907	7.2687	911	7.4287	914	7.5958	918	7.7704	922	7.9530	7
83	925	8.1443	929	8.3450	932	8.5555	936	8.7769	939	9.0098	942	9.2553	6
84	945	9.5144	948	9.7882	951	10.078	954	10.3835	957	10.711	959	11.059	5
85	962	11.430	964	11.826	967	12.250	969	12.706	971	13.197	974	13.727	4
86	976	14.300	978	14.924	980	15.605	981	16.350	983	17.169	985	18.075	3
87	986	19.081	988	20.206	989	21.470	990	22.903	992	24.542	993	26.432	2
88	994	28.636	995	31.242	996	34.368	997	38.189	997	42.964	998	49.104	1
89	9998	57.290	9999	68.750	9999	85.940	9999	114.58	1.000	171.88	1.000	343.77	0
deg.	60' cos	60' cot	50' cos	50' cot	40' cos	40' cot	30' cos	30' cot	20' cos	20' cot	10' cos	10' cot	deg.

TABLES FOR EXCAVATIONS AND EMBANKMENTS.

Distances from Center of Roadway for Cross-Sectioning.  
Roadway 18 Feet Wide. Side Slopes 1 to 1.  
For Single Track Excavation.

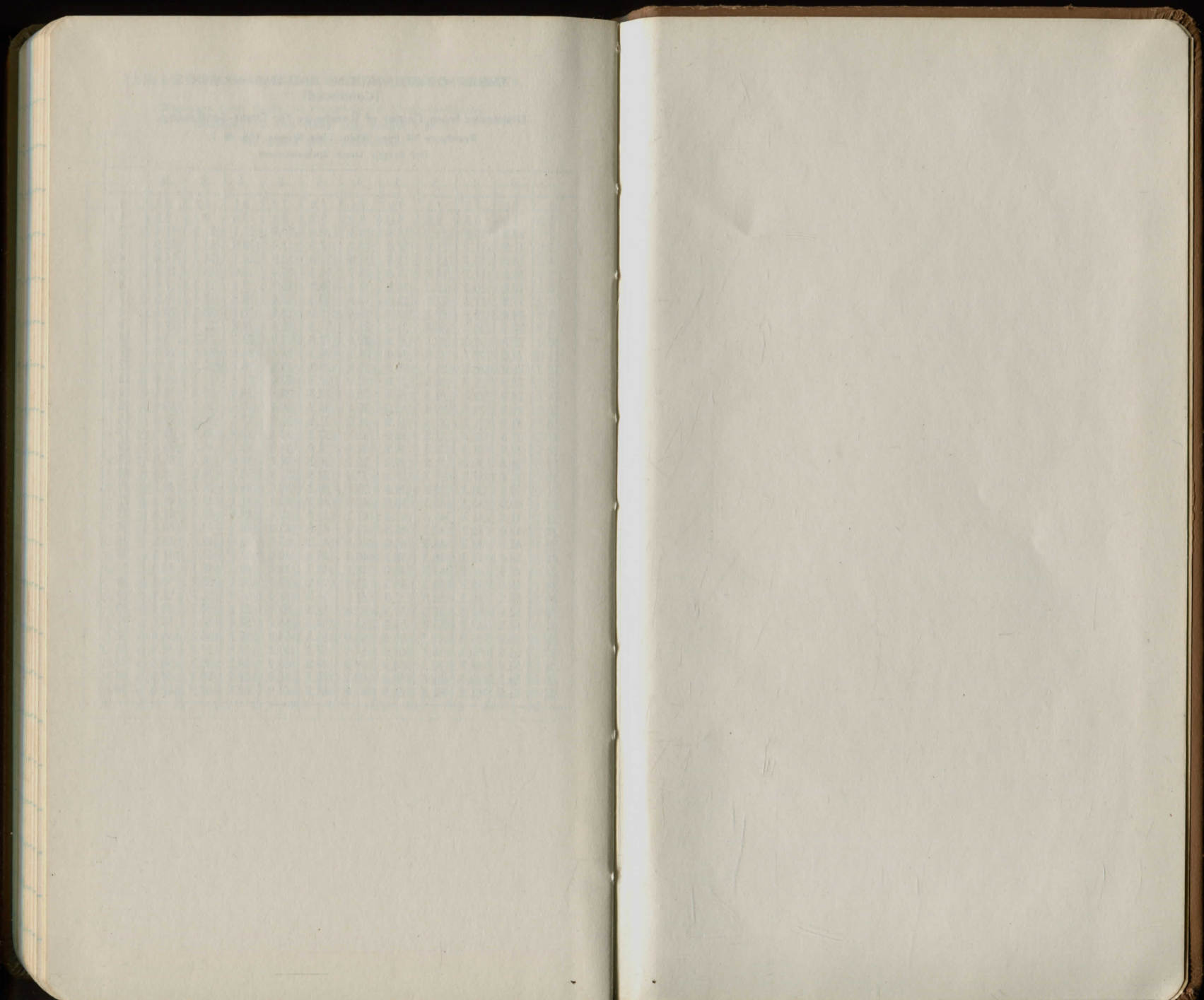
	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

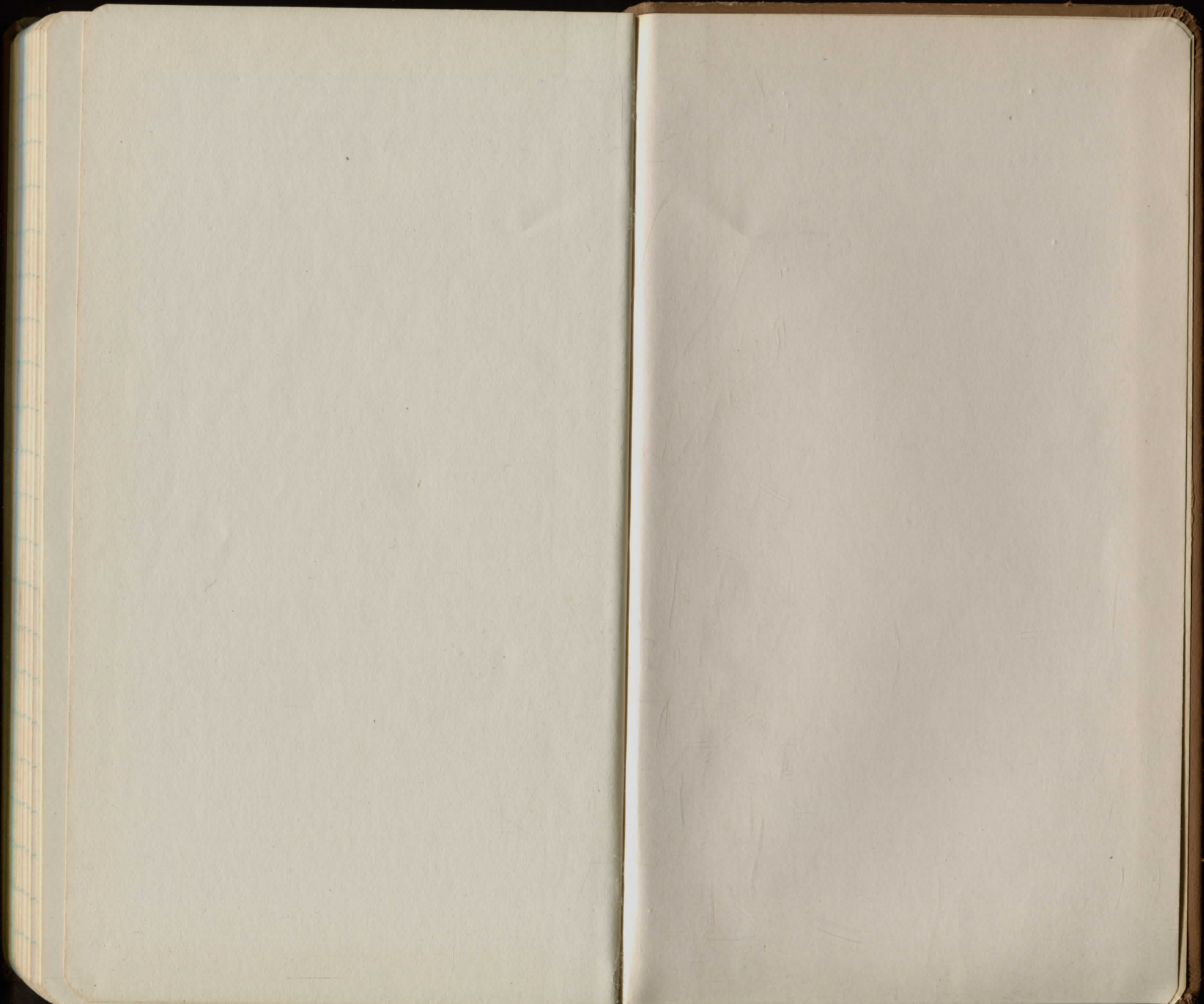
TABLES FOR EXCAVATIONS AND EMBANKMENTS

(Continued)

Distances from Center of Roadway for Cross-Sectioning.  
Roadway 14 Feet Wide. Side Slopes 1 1/2 to 1.  
For Single Track Embankment.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36





.200

50.53 } 690  
50.35 } .175  
          } .11

1.51 N

.125

.121

1.495 s     .215

15 3.855 sugar  
15.11     929.33  
42     915  
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      74.33

911.703  
   765  
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919.355 HI  
   4.37

914985 Top factor

929.33  
   786  
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937.19  
   3.63  
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933.56

919.355  
   947  
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918.408  
   646  
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914362  
   583  
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912579

915.  
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18.56

above 18-6<sup>3</sup>/<sub>4</sub> =  
17-6<sup>3</sup>/<sub>4</sub>

712.30  
   4.26

8.08

7114.865

705.1  
   2.4  
-----  
   0.275

